6911 Southpoint Drive (B03)
Burnaby, BC
V3N 4X8

July 30, 2024

[redacted]

Dear [redacted] :

RE: CEAP IR 42 - [redacted] - Interconnection Feasibility Study Report

Enclosed is the Interconnection Feasibility study report for the proposed [redacted] submitted under Attachment M-2: Transmission Service and Interconnection Service Procedures for Competitive Electricity Acquisition Process (CEAP) of the Open Access Transmission Tariff (OATT). This letter provides a non-binding good faith estimate of the cost and time to construct the facilities required to interconnect your project to BC Hydro's Transmission System, being the Network Upgrades, based on the findings of the Interconnection Feasibility study.

Open Access Transmission Tariff

The OATT defines Network Upgrades as additions, modifications, and upgrades to BC Hydro's Transmission System required at or beyond the Point of Interconnection to accommodate the interconnection of the Generating Facility to the BC Hydro's Transmission System. Pursuant to the OATT, BC Hydro will design, procure, construct, install, and own the Network Upgrades. While BC Hydro will pay the costs for the Network Upgrades, the Interconnection Customer provides security for such costs.

Cost Estimate

Based on the Interconnection Feasibility study, the non-binding good faith estimated cost (typical accuracy range of +150%/-50%) for Network Upgrades required to interconnect your project is $11.7 M.

Major Scope of Work Identified:

- Add one 138 kV line position with the associated substation equipment at BC Hydro's Highland (HLD) substation
- Relocate the connection of 1L55 with the associated station work
- Add and upgrade Protection, Control and Telecom

Exclusions:

- GST
- Right-of-Way (ROW)
- Permitting

Key Assumptions:

- Construction by contractor.
- 3 years of construction is considered
- Early Engineering and Procurement
- No expansion of existing stations or control buildings to accommodate new equipment

Key Risks:

- Expansion may be required of existing control building at HLD to accommodate new P&C panels
- Transmission routing may be different than assumed, including number of disconnect switches and structure types may change
- No defined supply chain strategy, construction costs may increase depending on delivery method
- Project schedule may be longer than expected, leading to increased costs
- Costs may be affected by market conditions and escalation
- Additional Right-of-Way (ROW) may be required

Please note that the Revenue Metering requirements and associated costs required to interconnect your project have not been determined at this stage and, therefore, not included in the above estimate. Revenue Metering costs that are attributable to the Interconnection Customer are to be paid in cash. For more details on Revenue Metering requirements and responsibilities, please refer to:

https://www.bchydro.com/content/dam/BCHydro/customer-portal/documents/distribution/standards/ds-rmr-complex-revenue-metering.pdf.

Schedule

Based on the Interconnection Feasibility study, the non-binding good faith estimated in-service date for your project's Network Upgrades is Quarter 3 2030 (calendar year). To achieve this timeline, we may need to expedite certain activities, including engineering design and procurement of long-lead equipment.

Timely actions required from you to minimize risks to the schedule:

- Submission of additional technical data required for the System Impact Study and Facilities Study
- Submission of any required information or document such as demonstration of Site Control
- Execution of Combined Study Agreement and Standard Generator Interconnection Agreement
- Financial commitments and securities

Please note that changes to your interconnection request, delays in data submission, or financial commitments may also impact the target in-service date.

Next Steps

In September 2024, we will issue a final invoice for the Feasibility Study costs. This invoice will reflect the total amount due, taking into account the $15,000 Feasibility Study deposit you have already paid and any remaining amount on the non-refundable $15,000 Interconnection request deposit that we did not spend in reviewing and validating your interconnection request.

If you have any questions, please contact the BC Hydro CEAP Team at ceap2024@bchydro.com.

Sincerely,

[redacted]

Senior Manager, Transmission Interconnections

BC Hydro

Encl.: CEAP2024_IR_42_[redacted]FeS_Report_final.pdf

[redacted] (POI at HLD)

Interconnection Feasibility Study

BC Hydro EGBC Permit to Practice No: 1002449

2024 CEAP IR # 42

Prepared for: [redacted]

[redacted]

[redacted]

Report Metadata

Header:	[redacted] (POI at HLD)
Subheader:	Interconnection Feasibility Study
Title:	[redacted] (POI at HLD)
Subtitle:	2024 CEAP IR # 42
Report Number:	300-APR-00010
Revision:	0
Confidentiality:	Public
Date:	2024 Jul 30
Volume:	1 of 1
Prepared for:	[redacted]

[redacted]

Related Facilities:	HLD
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Revisions

Revision	Date	Description
0	2024 Jul	Initial release

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Executive Summary

[redacted] the interconnection customer (IC), requests to interconnect its [redacted] (2024 CEAP IR # 42) to the BC Hydro (BCH) system. [redacted] has twenty-eight (28) inverters [redacted] adding a total capacity of 104 MW. The proposed Point of Interconnection (POI) is BC Hydro's 138 kV Highland Substation (HLD). The IC's project will connect to the POI via a 15km, 138 kV interconnection line. The IC's proposed commercial operation date (COD) is October 1, 2028.

To interconnect the [redacted] and its facilities to the BCH Transmission System at the proposed POI, this Feasibility Study has identified the following conclusions and requirements:

1. A new 138 kV line position (1LXXX) at HLD is required to interconnect the IC's generating project to the BC Hydro system.
2. The connection of [redacted] does not cause any performance violation (i.e. thermal overload, voltage performance violation or voltage stability concern) under system normal conditions.
3. The connection of [redacted] will cause an overload on 1L205 under single contingencies. If an overload on 1L205 is detected, a signal from HLD or SVA will be initiated to shed or run back generation at the IC's facility. The overload mitigation solution will be further explored in the next phase of the project.
4. In addition to entrance protection and 1LXXX line protection, the IC is required to install anti-islanding protection within their facility to disconnect the IC's wind farm from the grid when an inadvertent island with the local load forms.
5. According to BC Hydro's TIR, the IC's project must have sufficient reactive power capability over full MW operating range including at the zero MW output level. The [redacted] as submitted does not meet the reactive capability requirement at zero MW output level, which will need to be addressed.
6. New line protection relays will be added at BC Hydro's Highland Substation (HLD) and the IC's substation (P42) for the 138 kV interconnection line

between HLD and P42. BC Hydro will provide line protections at HLD. As part of the line protection addition, telecommunication facilities will be required between HLD and [redacted] (P42). The IC shall provide required relays, telecom facility and associated equipment at its facilities to accommodate the new protection schemes.

The above conclusions are made based on the IC's input data and study assumptions listed in Section 4, which represent the best available information on May 22, 2024.

A non-binding good faith estimated cost and time to construct the Network Upgrades required to interconnect the proposed project will be provided in a separate letter to the IC.

Contents

Appendices

Acronyms

The following are acronyms used in this report.

BCH	BC Hydro
CEAP	Competitive Electricity Acquisition Process
COD	Commercial Operation Date
DTT	Direct Transfer Trip
ERIS	Energy Resource Interconnection Service
FeS	Feasibility Study
IBR	Inverter-Based Resources
IC	Interconnection Customer
MPO	Maximum Power Output
NERC	North American Electric Reliability Corporation
NRIS	Network Resource Interconnection Service
OATT	Open Access Transmission Tariff
POI	Point of Interconnection
RAS	Remedial Action Scheme
TIR	BC Hydro "60 KV to 500 kV Technical Interconnection Requirements for Power Generators"
WECC	Western Electricity Coordinating Council
WTG	Wind Turbine Generator
EDM	Edmonds Office
FVO	Fraser Valley Office
SIO	South Interior Office

1 Introduction

Table 1-1 below summarizes the project reviewed in this Feasibility Study.

Table 1-1 Summary of Project Information

Project Name	[redacted] (POI at HLD)	
Name of Interconnection Customer (IC)	[redacted]	
Point of Interconnection (POI)	Highland Substation (HLD)	
IC's Proposed COD	1st October 2028	
Type of Interconnection Service	NRIS ☒	ERIS ☐
Maximum Power Injection [1] (MW)	102 MW (Summer)	102 MW (Winter)
Number of Generator Units	28 x 3.71 MW	
Plant Fuel	Solar	

[redacted] the interconnection customer (IC), requests to interconnect its [redacted] (2024 CEAP IR # 42) to the BC Hydro system. [redacted] has twenty-eight (28) inverters [redacted], with total installed capacity of 104 MW. The IC's proposed Point of Interconnection (POI) is BC Hydro's 138 kV Highland Substation (HLD). The IC's project will connect to the POI via a 15 km 138 kV interconnection line. The IC's proposed commercial operation date (COD) is October 1st, 2028.

Figure 1-1 shows the Nicola-Highland region transmission system diagram. Nicola substation (NIC) is a major substation in this area with two existing 500/230 kV transformers (NIC T2 & T3) and two 230/138 kV transformers (NIC T5 & T6). NIC presently supplies three 138 kV transmission lines — 1L251 to the [redacted] Copper Mountain substation (CUM) and Similco substation (SCO), 1L243 to BC Hydro's Highland substation (HLD) and 1L244 to BC Hydro's Westbank substation (WBK).

[redacted]

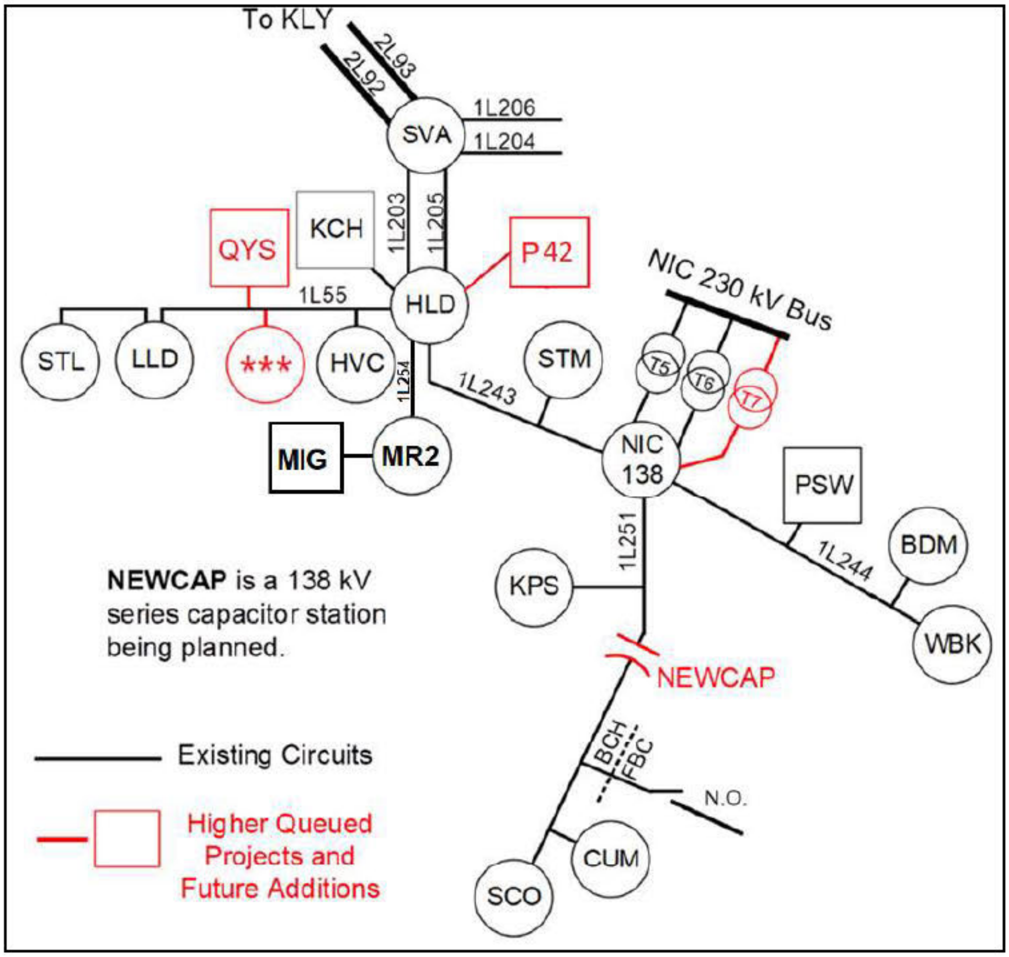

Figure 1-1: Nicola-Highland region 138/230 kV Transmission System Diagram

HLD is a 138/60 kV substation that mainly supplies the industrial customer of Highland Valley Copper. It also interconnects two power plants owned by independent power producers (IPP) in the region:

- Kwoiek Creek Generating Station (KCH) with a total capacity of 60 MW is connected to HLD via a 72.7 km, 138 kV transmission line 1L57.
- Merritt Green Energy Project Generating Station (MIG) with a total capacity of 40 MW is connected to Merritt 2 Substation (MR2) which is fed by 1L254 from HLD.

In addition to these existing IPPs, quA-ymn Solar farm (QYS) is a 15 MW IPP generating project under construction in the region. It will connect to BC Hydro system via a tap on 1L55 at approximately 22.5 km from HLD.

There are several high-queued load interconnections and their associated network upgrades in the study area. The relevant network upgrades being planned in the study region are as follows.

- Nicola Substation Transformation Capacity Reinforcement: this project will add a new 230 kV/138 kV transformer at NIC (i.e. NIC T7) to mitigate the possible transformer overload associated with the industrial load increase in Highland region.
- 1L243 reconductoring: this line rating upgrade is required to accommodate an industrial load increase in Highland region.
- 1L251 series capacitor project: Line 1L251 will be series compensated to accommodate an industrial load increase on 1L251.

2 Purpose and Scopes of Study

This Feasibility Study is a preliminary evaluation of the system impact of interconnecting the proposed project to the BC Hydro system based on power flow and short circuit analysis in accordance with BCH's Open Access Transmission Tariff (OATT). A non-binding good faith estimated cost of required Network Upgrades and estimated time to construct will be provided.

Per OATT, the feasibility study is performed individually for each of the participating projects in the CEAP process and focuses specifically on the BC Hydro regional transmission system where the proposed generating project is proposed to be constructed. An assessment of the incremental effect on the 500kV bulk transmission system is beyond this study scope.

This is a "limited scope" study which is restricted to power flow studies of P0, P1, and P2 planning events as defined in TPL-001-4 Table 1 and short circuit analysis. The study does not address other technical aspects such as transient stability and switching transients and impact of multiple contingencies. These subjects would be addressed in subsequent System Impact Study if the project is a Successful Participant of the CEAP.

In case impact to the adjacent external systems to BC Hydro is observed, such impact would be addressed in subsequent detailed and coordinated studies with the relevant adjacent entities if the proposed interconnection proceeds further.

3 Standard and Criteria

The Feasibility Study is performed in compliance with the North American Electric Reliability Corporation (NERC) and Western Electricity Coordinating Council (WECC) reliability standards, and the BCH interconnection requirements in the TIR, and upon the ratings of the existing BCH transmission facilities described in Operating Orders, specifically:

- NERC standards: TPL-001-4 and FAC-002-3 relevant to the scope of this Feasibility Study.
- WECC criteria TPL-001-WECC-CRT-4 Transmission System Planning Performance, July 1, 2023.
- BC Hydro's 60 kV to 500 kV Technical Interconnection Requirements for Power Generators.
- BC Hydro Operating Order 5T-10, Ratings for All Transmission Circuits 60 kV or Higher, April 16, 2024.
- BC Hydro Operating Order 5T-14, Ratings for All Transmission and Distribution Transformer, November 8, 2022.
- BC Hydro System Operating Order 7T-22 System Voltage Control, September 19, 2023.

4 Assumptions and Conditions

This Feasibility Study is performed based on the IC's submitted data and information available to BC Hydro on May 22, 2024 for the study purpose. Appendix A shows the plant single line diagram for the IC's project used in the study model. Certain assumptions were, as set out below, made to the extent required.

The power flow study cases used in this Feasibility Study are established based upon the BC Hydro's base resource plan and load forecasts available at the time of performing the study, which includes existing and future generations, transmission facilities, and loads in addition to the subject interconnection project in this study. Applicable seasonal conditions and the appropriate study years for the study planning horizon are also incorporated.

Additional assumptions are listed as follows.

1) The regional generation are dispatched to the patterns that stress the transmission system in the study area. In these patterns, the regional generations are typically set to their Maximum Power Outputs (MPO) unless otherwise specified.

2) West Kelowna Transmission Project (WKTP) is not included in the Feasibility Study model, as the project scope is undetermined at the time of performing this study.

3) For the purpose of performing this study, Nicola Substation Transformation Capacity Reinforcement project (i.e. addition of NIC T7) and 1L243 reconductoring is assumed completed by the time the IC's generating project enters service.

4) 1L243 after reconductoring is assumed to have a conductor rating of 1145 A (summer) and 1388 A (winter).

5) The projected in-service date for 1L251 series capacitor project is not available. For the sole purpose of delivering this Feasibility Study, it is assumed the series capacitor will enter service in early 2028.

5 System Studies and Results

5.1 Power Flow Study Results

Power flow studies were performed to evaluate whether the IC's generating project would cause any unacceptable system performance (e.g. equipment overloads, steady-state voltage violation and voltage instability) and to determine the reinforcement requirement based on steady state performance analysis.

The study focuses on the 2029 light summer (29LS) system load condition which is typically a stressed condition for a generation interconnection project, taking into considerations of factors such as load conditions, seasons and generation patterns. The 2029 heavy summer (29HS) and 2028 heavy winter (28HW) cases are also checked at a high level to capture any possibility of performance violations under high load conditions.

5.1.1 Branch Loading Analysis

Table 5-1 shows a summary of branch loading analysis under system normal and single contingencies (Categories P1 and P2) for various load conditions.

For all the studied load conditions (28HW, 29HS, and 29LS), there is no branch overload identified under system normal condition (Category P0). Line 1L205 overload is observed in 29LS case under HLD 1CB4 contingency (Category P2.3 event).

With high outputs from Highland region IPPs and light summer load condition, there could be a slight overload (~103%) as indicated in Table 3-1 on 1L205 under HLD 1CB4 contingency (which trips both 1L55 and 1L203). This line overload is due to the interconnection of the IC's Project. Line 1L205 has an emergency overload rating for 30 minutes at 111% above its normal capacity and to address the potential overload due to HLD 1CB4 contingency, one viable solution is to reduce power generation at the Customer's site through a runback RAS or operator intervention within 30 minutes of the contingency. The solution will be further explored in the next phase of the project.

Table 5-1: Summary of Branch Loading Analysis Results

Case	IC's Plant Output	Contingency		Branch Loading		
				1L243	1L203	1L205
		Cat.	Description	HLD-NIC	HLD-SVA	HLD-SVA
Winter Rating				331.8 MVA	191.2 MVA	149.6 MVA
28HW	Max	P0	System Normal	6.6%	25.2%	30.6%
	Max	P1	1L203	10.8%	-	49.4%
	Max	P2	HLD_1CB4	22.4%	-	71.7%
Summer Rating				273.7 MVA	172.8 MVA	118.6 MVA
29HS	Max	P0	System Normal	5.6%	31.6 %	43.6%
	Max	P1	1L203	11.5%	-	70.8%
	Max	P2	HLD_1CB4	26.1%	-	98.7%
29LS	Max	P0	System Normal	6.8%	34.2%	47.3%
	Max	P1	1L203	13.8%	-	77.1%
	Max	P2	HLD_1CB4	27.5%	-	**103.1%**

5.1.2 Steady-State Voltage Analysis

With the connection of the IC's project, the voltage performance under system normal condition and single contingencies is acceptable for all the three load conditions (29LS, 29HS, 28HW). Table 5-2 shows a summery of steady-state voltage performance under various system conditions and contingencies.

Table 5-2: Summary of Steady-State Voltage Study Results

Case	IC's Plant Output	Contingency		Bus Voltage (PU)		
		Cat.	Description	HLD 138	SVA 138	WKA 138
28HW	Max	P0	System Normal	1.01	1.02	1.01
	Max	P1	1L203	1.00	1.02	1.01
	Max	P2	HLD_1CB4	1.02	1.02	1.01
29HS	Max	P0	System Normal	1.00	1.02	1.01
	Max	P1	1L203	1.00	1.02	1.01
	Max	P2	HLD_1CB4	1.02	1.02	1.01
29LS	Max	P0	System Normal	1.01	1.02	1.01
	Max	P1	1L203	1.00	1.02	1.01
	Max	P2	HLD_1CB4	1.02	1.02	1.01

5.1.3 Reactive Power Capability Evaluation

The BC Hydro TIR requires IBR power plant to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range.

Based on the PSS/E power flow data submitted by the IC, the proposed generating project would be capable of to meet the BC Hydro's reactive capability requirement at the plant's maximum MW output, which is subjected to further verification in the next stage of interconnection study.

Furthermore, the BCH TIR requires the IC's project to provide sufficient reactive power capability over full MW operating range including at zero MW output level. The proposed wind farm does not meet this requirement at near zero MW output, which will need to be addressed.

5.1.4 Anti-Islanding Requirements

The IC is required to install anti-islanding protection within its facility to disconnect the IC's wind farm from the grid when an inadvertent island with the local load forms.

5.2 Fault Analysis

The short circuit analysis in the FeS is based upon the latest BC Hydro system model, which includes the generating facility information and associated impedance data provided by the IC. A more detailed study will be performed at the system impact study stage if needed.

5.3 Stations Requirements

The following station work is required at HLD:

- Relocate the connection of 1L55 with the associated station work per the one-line sketch in Appendix B.
- Add one 138 kV line position with the associated substation equipment. Refer to the one-line sketch in Appendix B for details.
- Expand the existing control building, if required, to accommodate the new P&C panels and other equipment.
- Terminate the 138 kV [redacted] transmission line.
- The location of metering will be determined in the next stage.
- Other associated station work.

5.4 Protection & Control Requirements

New line protection relays will be added at BC Hydro's Highland Substation (HLD) and the IC's substation (P42) for the 138 kV interconnection line between HLD and P42. BC Hydro will provide line protections at HLD. As part of the line protection addition, telecommunication facilities will be required between HLD and the IC's substation (P42).

The IC is to provide the following for the interconnection [redacted] (P42) to HLD:

- Entrance protection that complies with the latest version of the "60 kV to 500 kV BC Hydro Technical Interconnection Requirements for Power Generators."
- Provide two SEL-411L-1 relays (firmware and options specified by BC Hydro) at the entrance of P42 to provide protection coverage for the interconnection line between HLD and P42. BC Hydro P&C Planning will provide core protection settings for these relays to protect transmission line 1LXXX during a transmission line fault. Non-core protection such as local breaker failure, auto-reclosing, backup protection for station elements will not be provided by BC Hydro P&C Planning.
- The IC is responsible for NERC PRC-related tasks, settings to compliance standards within their facilities.
- The IC is responsible for providing a communications link for remote interrogation of the PPIS equipment by BCH servers.
- Provide anti-islanding protection as stated in Section 5.1.

The runback schemes or RAS requirements stated in Section 5.1 are mainly to address the overloading concerns under contingencies, which are preliminary. These RAS requirements may utilize the communication channels required for protection purposes included in the cost estimate. If the proposed project proceeds through the CEAP process, subsequent System Impact Studies may identify additional RAS requirements for this interconnection. These RAS functional requirements will include initiating events, control actions, and latency times. Depending on these supplementary requirements, additional telecommunication facilities may be needed to facilitate signal transmission between the BC Hydro substations and customer facilities.

5.5 Telecommunications Requirements

BC Hydro performed a high-level feasibility assessment of a telecom solution to meet the following requirements.

Teleprotection Requirements for Telecom

- Provide WECC Level 3 64 kbps synchronous circuits between HLD and P42. Physical interface shall be C37.94 optical over multimode fibre using ST connectors.

Telecontrol Requirements for Telecom

- P42 SCADA circuits to FVO and SIO would be provided using either a virtual private network tunnel over a business grade Internet service, or an E-line leased line.

Other Requirements for Telecom

- None identified.

Certain assumptions were made for determining a potential telecom solution. Details of the telecom solution (e.g. assumptions made, alternatives investigated and work required for BCH and the IC) would be provided at the next study stage.

6 Cost Estimate and Schedule

The non-binding good faith estimated cost and time to construct the Network Upgrades required to interconnect the proposed project will be provided in a separate letter to the IC.

7 Conclusions

To interconnect the [redacted] and its facilities to the BCH Transmission System at the POI, this Feasibility Study has identified the following conclusions and requirements:

1. A new 138 kV line position at HLD is required to interconnect the IC's generating project to the BC Hydro system.

2. The connection of [redacted] does not cause any performance violation (i.e. thermal overload, voltage performance violation or voltage stability concern) under system normal conditions.

3. The connection of [redacted] will cause an overload on 1L205 under single contingencies. If an overload on 1L205 is detected, a signal from HLD or SVA will be initiated to shed or run back generation at the IC's facility. The overload mitigation solution will be further explored in the next phase of the project.

4. In addition to entrance protection and 1LXXX line protection, the IC is required to install anti-islanding protection within their facility to disconnect the IC's wind farm from the grid when an inadvertent island with the local load forms.

5. According to BC Hydro's TIR, the IC's project must have sufficient reactive power capability over full MW operating range including at the zero MW output level. The [redacted] as submitted does not meet the reactive capability requirement at zero MW output level, which will need to be addressed.

6. New line protection relays will be added at BC Hydro's Highland Substation (HLD) and the IC's substation (P42) for the 138 kV interconnection line between HLD and P42. BC Hydro will provide line protections at HLD. As part of the line protection addition, telecommunication facilities will be required between HLD and [redacted] (P42). The IC shall provide required relays, telecom facility and associated equipment at its facilities to accommodate the new protection schemes.

Appendix A
Plant Single Line Diagram Used for Power Flow Study

Figure A-1 shows [redacted] (POI at HLD) single line diagram used for power flow study.

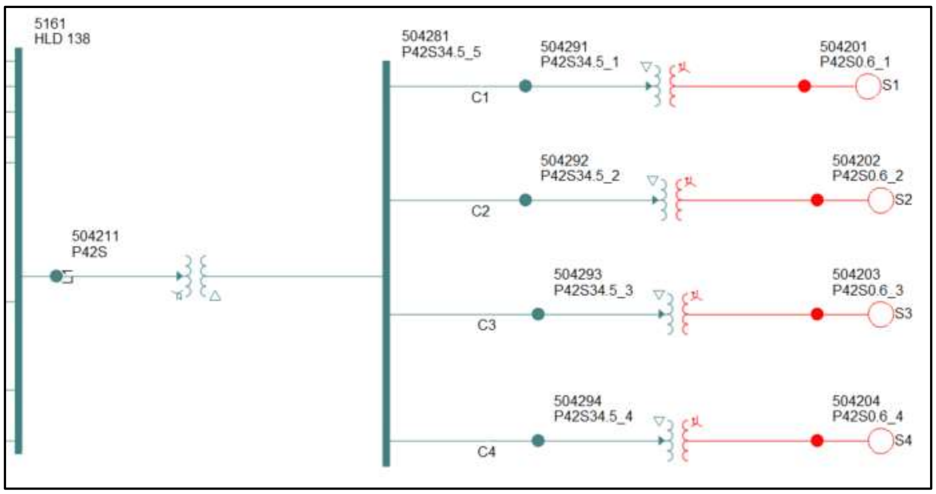

Figure A-1: [redacted] (POI at HLD) Single Line Diagram for Power Flow Study.

As seen in the diagram, [redacted] (POI at HLD) has a main power transformer to connect four (4) feeders which connected with solar inverters.

Appendix B

One-Line Sketch for the Development of HLD

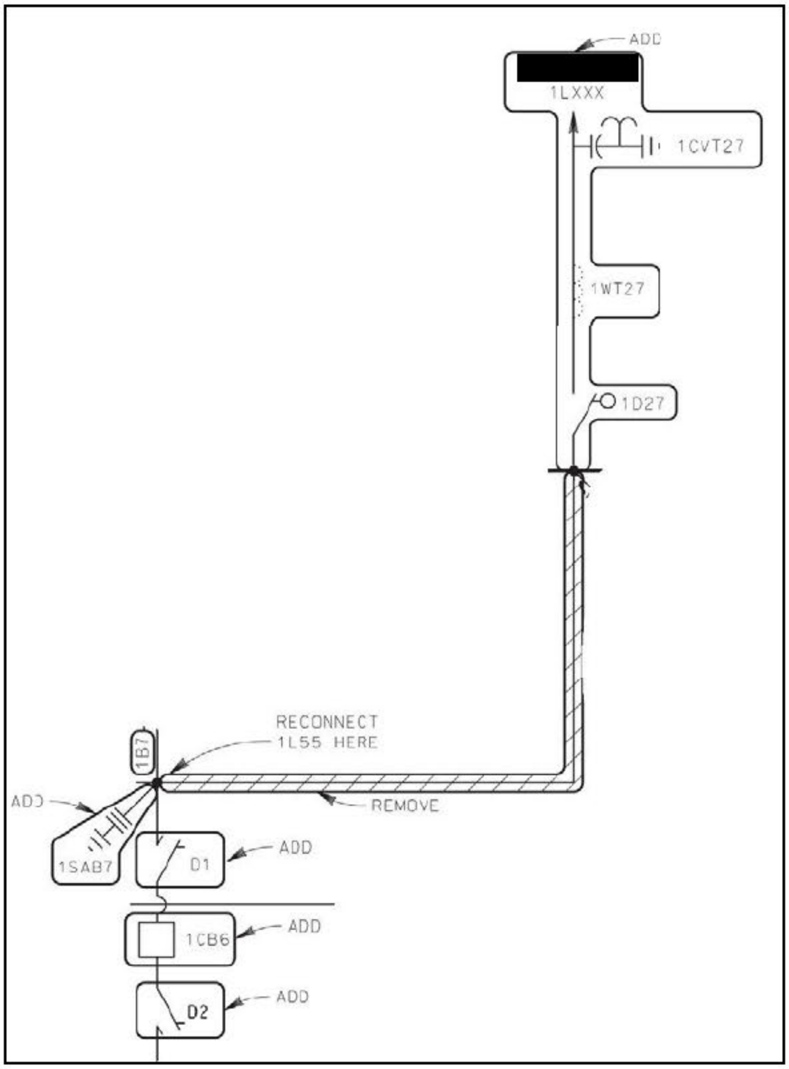

Figure B-1: One Line Sketch for the Development of HLD