6911 Southpoint Drive (B03)
Burnaby, BC
V3N 4X8

November 24, 2025

[redacted]

via email: [redacted]

RE: CEAP IR #96 – [redacted] – Interconnection Feasibility Study

Dear [redacted]

Enclosed is the Interconnection Feasibility Study for the proposed Interconnection Request (IR), [redacted], submitted under Attachment M-2: Transmission Service and Interconnection Service Procedures for Competitive Electricity Acquisition Process (CEAP) of the Open Access Transmission Tariff (OATT). This letter provides a non-binding good faith estimate of the cost and time to construct the facilities required to interconnect your project to BC Hydro's Transmission System, being the Network Upgrades, based on the findings of the Interconnection Feasibility Study.

Open Access Transmission Tariff

The OATT defines Network Upgrades as additions, modifications, and upgrades to BC Hydro's Transmission System required at or beyond the Point of Interconnection to accommodate the interconnection of the Generating Facility to the BC Hydro's Transmission System. Pursuant to the OATT, BC Hydro will design, procure, construct, install, and own the Network Upgrades. While BC Hydro will pay the costs for the Network Upgrades, the Interconnection Customer provides security for such costs.

Interconnection Study Costs

The Interconnection Customer is responsible for paying the full cost of all Interconnection Studies in cash. Interconnection Study costs vary depending on the scope, complexity, and other factors such as whether any scope is shared with another Interconnection Customer (not applicable to this Interconnection Feasibility Study). The deposit amounts specified in the OATT are not proxy Interconnection Study costs. If actual Interconnection Study costs exceed the deposit amount, the Interconnection Customer must pay the remaining balance in cash. Please refer to the answer for question no. 53 in the posted Questions & Answers for 2025 Call for Power for typical study cost ranges.

Cost Estimate

Based on the Interconnection Feasibility Study, the non-binding good faith estimated cost (typical accuracy range of +150%/-50%) for Network Upgrades required to interconnect your project is $34.7 M.

Major Scope of Work Identified:

- Add one 230 kV line position and one terminal with associated substation equipment at BC Hydro Nicola substation (NIC)
- Add station equipment such as one circuit breaker, 3 manual disconnect switches, one motor operated switch, instrument transformers, and one surge arrester

- Upgrade required substation facilities, infrastructures, and bus work to support new station equipment
- Terminate the 230kV line of [redacted] Project at the station
- Supply and install required Protection, Control and Telecommunications equipment

Exclusions:

- GST
- Permits
- Right-of-Way & property costs

Key Assumptions:

- Construction by contractor
- 24 months of construction is considered
- No construction during winter season
- Execution of early Engineering and Procurement Agreement
- No expansion of existing stations or control buildings to accommodate new equipment
- Impact Benefit Agreements with First Nations are not considered

Key Risks:

- Expansion of the existing station and/or control building may be required leading to increased costs and/or a longer project schedule
- Major equipment delivery presents potential project cost and schedule risks, based on variance in equipment lead times
- No defined supply chain strategy; construction costs may increase depending on delivery method
- Project schedule may be longer than expected, leading to increased overhead costs
- Ground improvements may be required leading to increased construction costs
- Contaminated soil may be encountered leading to increased construction costs
- Cost of materials and major equipment may be affected by market conditions and escalation

Study Limitations and Exclusions

Protection, Control, and Telecommunications

The Interconnection Feasibility Study does not include a detailed review of the protection, control, and telecommunications system requirements specific to your Interconnection Request. Based on a high-level review, we have identified proxy costs for protection, control, and telecom Network Upgrades drawn from comparable interconnection projects with similar scope and complexity; these proxy costs have been included solely for indicative budgeting purposes. The relative interconnection cost determined by the Interconnection Feasibility Study includes a telecommunications component based on an assumed solution to deliver teleprotection and telecontrol circuit requirements necessary for the Interconnection Request. Protection, control, and telecommunications system requirements will be reviewed in detail in the System Impact Study if you are a successful participant of the CEAP and meet applicable requirements.

For Interconnection Feasibility Study purposes, it is assumed that any applicant-proposed works that could obstruct or impair the performance of existing BC Hydro microwave systems or new links from the proposed Interconnection Customer Interconnection Facilities (ICIF) to the BC Hydro microwave system would be identified and either relocated or repositioned as determined in a System Impact Study if you are a successful participant of the CEAP and meet applicable requirements. Such works may include, but are not limited to, towers, turbines, dams, support structures, panels, surface materials deposited or redistributed, water surface changes, or vegetation.

Generation Shedding/Curtailment Scheme and Electromagnetic Transient (EMT) Studies

The generation shedding/curtailment scheme reviews (e.g., Remedial Action Scheme (RAS), and a direct transfer trip for anti-islanding scheme) and EMT studies are completed in a System Impact Study. The outcomes of these studies may result in additional requirements, which could include Network Upgrades or ICIF. Any costs associated with completion of these studies, and resulting requirements, are not included in the Interconnection Feasibility Study cost estimate.

Revenue Metering

Please note that revenue metering requirements have not been determined with the Interconnection Feasibility Study. As such, any costs associated with revenue metering and other interconnection components are not included in the cost estimate provided above. Once these requirements are defined, costs that are attributable to the Interconnection Customer are to be paid in cash. For more details on revenue metering requirements and responsibilities, please refer to:

https://www.bchydro.com/content/dam/BCHydro/customer-portal/documents/distribution/standards/ds-rmr-complex-revenue-metering.pdf.

Schedule

Based on the Interconnection Feasibility Study, the non-binding good faith estimated in-service date for your Interconnection Request's Network Upgrades is Quarter 3 2031 (calendar year). To achieve this timeline, we may need to expedite certain activities, including engineering design and procurement of long-lead equipment.

Timely actions required from you to minimize risks to the schedule:

- Submission of additional technical data required for the System Impact Study and Facilities Study
- Submission of any required information or document such as demonstration of Site Control
- Execution of Combined Study Agreement and Standard Generator Interconnection Agreement
- Financial commitments and securities

Please note that changes to your Interconnection Request or delays in data submission or financial commitments may also impact the target in-service date.

If you have any questions, please contact the BC Hydro CEAP team at ceap2025@bchydro.com.

Sincerely,

[redacted]

[redacted]

Manager, Customer Interconnections

BC Hydro

Encl.: CEAP_2025_IR96_[redacted]_Feasibility_Study.pdf

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[redacted]

Interconnection Feasibility Study

BC Hydro EGBC Permit to Practice No: 1002449

2025 CEAP IR # 96

Prepared for: [redacted]

Prepared by: [redacted]

[redacted]

[redacted]
Sr. Engineer, Interconnection Planning

Reviewed by: [redacted]
Manager, Interconnection Planning

Accepted by: [redacted]
Manager, Transmission Planning

300-APR-00053
2025 Nov 21

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Prepared for:	[redacted]
Prepared by:	[redacted]
Title:	Sr. Engineer, Interconnection Planning
Checked by:	[redacted]
Title:	Specialist Engineer, Interconnection Planning
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Title:	Manager, Interconnection Planning
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Revision	Date	Description
0	2025 Nov	Initial release

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Entire report except listed below | Transmission Planning

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[redacted]

Sr. Engineer, Interconnection Planning

[redacted]

Section: | **Discipline:**

5.2, 5.3 | Stations Planning

Contributed by:

[redacted]

[redacted]

Engineer, Station Planning

[redacted]

Executive Summary

[redacted], the interconnection customer (IC), requests to interconnect its [redacted] project (2025 CEAP IR # 96) to the BC Hydro (BCH) system. [redacted] hereafter [redacted], has sixty (60) [redacted] type-4 wind turbine generators with total installed capacity of 252 MW. The proposed Point of Interconnection (POI) is at BC Hydro's Nicola substation (NIC). The IC's project will connect to the proposed POI via a 100 km, 230 kV interconnection line. The IC's proposed commercial operation date (COD) is July 7, 2030.

To interconnect the [redacted] and its facilities to the BCH Transmission System at the proposed POI, this Feasibility Study has made the recommendations and conclusions as follow:

1. A new 230 kV line position is required at NIC substation to facilitate the interconnection of [redacted].
2. The connection of [redacted] does not cause any performance violation (i.e. thermal overload, voltage performance violation or voltage stability concern) under system normal conditions.
3. Under critical single system contingency (N-1) conditions, the study has observed thermal overloads on 1L203, 1L205, 1L244_A, 1L244_B and SVA T3. The [redacted] may need to participate in the generation runback or shedding remedial action scheme (RAS) to maintain the system security. The RAS function scope will be specified in the System Impact Study (SIS) if the need for RAS is determined.
4. [redacted] is required to install anti-islanding protection within its facility to disconnect the IC's generating plant from the grid when an inadvertent island with the local load forms. The anti-islanding protection shall be configured in the manner that does not compromise the required fault ride-through performance.
5. The [redacted] is required to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range, per BC Hydro's TIR Section 6.4.2.

6. The "Extended Range with Reactive power at Standstill" for the proposed WTGs, as described in the Generation Capability Curve plot from Generator Capability Curve (Wind).pdf file, is required so that each turbine can provide reactive power capability at zero MW output. BC Hydro recognizes that the proposed Type-4 WTGs with the "Extended Range with Reactive power at Standstill" have an inherent limitation—providing only partial required reactive power capability during turbine standstill.
7. Fast Frequency Response is required at the [redacted]. The proposed wind turbine generators, when equipped with the FFR function, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The FFR settings should be determined in coordination with BC Hydro in the later stage of the interconnection process.

The above conclusions are made based on the IC's input data and study assumptions listed in Section 4, which represent the best available information on October 14, 2025.

A non-binding good faith estimated cost for required network upgrades and estimated schedule for construction are included in a separate letter to the IC.

Please note that, this Feasibility Study report does not include the descriptions of Protection, Control, and Telecommunications requirements and the associated upgrade scopes; however, as discussed in Section 2 "Purpose and Scopes of Study", the associated cost implications are captured and delivered in the cover letter to the IC.

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Contents

Appendices

Acronyms

The following are acronyms used in this report.

[redacted]	[redacted] Substation
CEAP	Competitive Electricity Acquisition Process
COD	Commercial Operation Date
DTT	Direct Transfer Trip
ERIS	Energy Resource Interconnection Service
FeS	Feasibility Study
[redacted]	[redacted] Substation
IBR	Inverter-Based Resources
IC	Interconnection Customer
IR	Interconnection Request
IPP	Independent Power Producer
[redacted]	[redacted] Substation
LAPS	Local Area Protection Schemes
[redacted]	[redacted] Substation
MPO	Maximum Power Output
NERC	North American Electric Reliability Corporation
NIC	Nicola Substations
NRIS	Network Resource Interconnection Service
OATT	Open Access Transmission Tariff
POI	Point of Interconnection
QYS	quA-ymn Solar farm Substation
RAS	Remedial Action Scheme
[redacted]	[redacted] Substation
TIR	BC Hydro “60 KV to 500 kV Technical Interconnection Requirements for Power Generators”
WECC	Western Electricity Coordinating Council
WKTP	West Kelowna Transmission Project
WTG	Wind Turbine Generator

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1 Introduction

Table 1-1 below summarizes the project reviewed in this Feasibility Study.

Table 1-1 Summary of Project Information

Project Name	[redacted]	
Name of Interconnection Customer (IC)	[redacted]	
Point of Interconnection (POI)	Nicola Substation (230 kV Side)	
IC's Proposed COD	July 7, 2030	
Type of Interconnection Service	NRIS ☒	ERIS ☐
Maximum Power Injection (MW)	238.6 MW (Summer)	238.6 MW (Winter)
Number of Turbines	60 WTGs	
Plant Fuel	Wind	

[redacted] the interconnection customer (IC), requests to interconnect its [redacted] (2025 CEAP IR: # 96) to the BC Hydro system. [redacted] hereafter [redacted], has sixty (60) [redacted] type-4 wind turbine generators with total installed capacity of 252 MW. The IC's proposed Point of Interconnection (POI) is on the 230 kV side of BC Hydro's Nicola substation (NIC). The IC's project will connect to the proposed POI via a 100 km, 230 kV interconnection line. The proposed commercial operation date (COD) is July 7, 2030.

Figure 1-1 shows the Nicola region transmission system diagram. Nicola substation (NIC) is a major substation in this area with two existing 500/230 kV transformers (NIC T2 & T3) rated at 1200 MVA each and two 230/138 kV transformers (NIC T5 & T6) rated at 300 MVA each. NIC presently supplies three 138 kV transmission lines — 1L251 to the [redacted] Copper Mountain substation (CUM) and Similco substation (SCO), 1L243 to BC Hydro's Highland substation (HLD) and 1L244 to BC Hydro's Westbank substation (WBK).

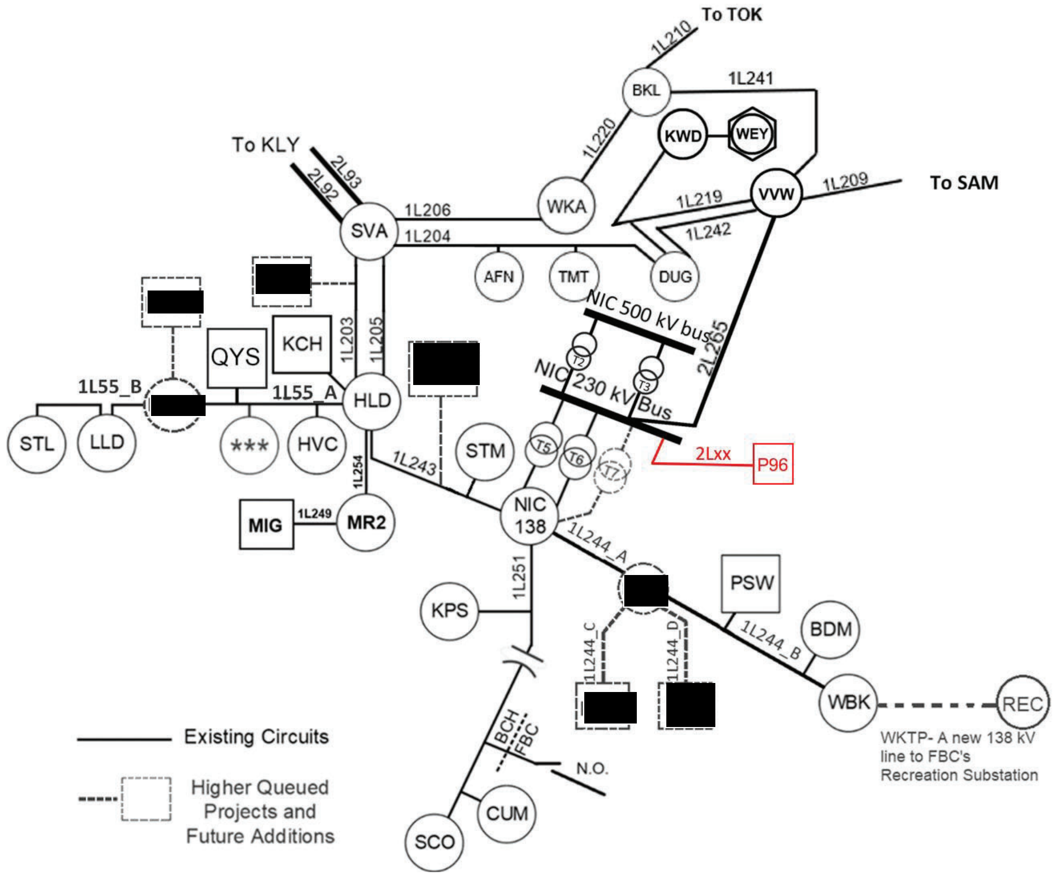

Figure 1-1: Nicola region 138/230 kV Transmission System Diagram

The Nicola region presently has four non-BCH generating facilities below.

- Pennask-Shinish Wind Farm (PSW);
- Kwoiek Creek Generating Station (KCH);
- Merritt Green Generating Station (MIG); and
- quA-ymn Solar farm (QYS).

In addition to the existing generators, the SIW region has five (5) proposed generating projects with higher queue priority — [redacted]. Together, these five projects represent nearly 700 MW of generating capacity addition to the region.

There are several transmission system reinforcements being planned in the study region as follows.

- Nicola Substation Transformation Capacity Reinforcement: this project will add a new 230 kV/138 kV transformer at NIC (i.e. NIC T7) to mitigate the potential transformer overload associated with the industrial load increase in Highland region.
- 1L243 reconductoring: this line rating upgrade is required to accommodate an industrial load increase in Highland region.
- 1L251 series capacitor project: Line 1L251 will be series compensated to accommodate an industrial load increase on 1L251.

2 Purpose and Scopes of Study

This Feasibility Study is a preliminary evaluation of the system impact of interconnecting the proposed project to the BC Hydro system based on power flow and short circuit analysis in accordance with BCH's Open Access Transmission Tariff (OATT) and produces the estimated cost of required Network Upgrades and the implementation schedule.

Per OATT, the Feasibility Study is performed individually for each of the participating projects in the CEAP process and focuses specifically on the BC Hydro regional transmission system where the proposed generating project is connected and affects.

This is a "limited scope" study which is restricted to power flow studies of P0, P1 and P2 planning events as defined in TPL-001-4 and short circuit analysis. The study does not address other technical aspects such as transient stability and switching transients and impact of multiple contingencies. These subjects will be addressed in subsequent System Impact Study if the project proceeds further. In addition, any potential impacts to the adjacent external systems to BC Hydro would be addressed in subsequent detailed and coordinated studies with the relevant adjacent entities if the proposed generator project proceeds further.

Please note that, due to the compressed study timeline for 2025 CEAP Feasibility Study, this report does not include the descriptions of the Protection, Control, and Telecommunication requirements and the associated upgrade scopes. Instead, the network upgrades associated with Protections, Controls and Telecommunications are incorporated with cost estimates in a separate cover letter to the IC.

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3 Standard and Criteria

The Feasibility Study is performed in compliance with the North American Electric Reliability Corporation (NERC) and Western Electricity Coordinating Council (WECC) reliability standards, and the BCH interconnection requirements in the TIR, and upon the ratings of the existing BCH transmission facilities described in Operating Orders, specifically:

- NERC standards: TPL-001-4 and FAC-002-3 relevant to the scope of this Feasibility Study.
- WECC criteria TPL-001-WECC-CRT-4 Transmission System Planning Performance, July 1, 2023.
- BC Hydro’s 60 kV to 500 kV Technical Interconnection Requirements for Power Generators, Rev 2.1.1, Effective: Sept 22, 2025.
- BC Hydro Operating Order 5T-10, Ratings for All Transmission Circuits 60 kV or Higher, Sept 17, 2025.
- BC Hydro Operating Order 5T-14, Ratings for All Transmission and Distribution Transformer, Sept 22, 2025.
- BC Hydro System Operating Order 7T-22 System Voltage Control, Sept 19, 2023.

4 Assumptions and Conditions

This Feasibility Study is performed based on the IC's submitted data and information available to BC Hydro on Oct 14, 2025, for the study purpose. Assumptions are made wherever the IC's input is unavailable. Appendix A shows the schematic diagram of the IC's project used in the study model.

The power flow study cases used in this Feasibility Study are established based upon the BC Hydro's base resource plan and load forecasts available at the time of performing the study, which includes existing and future generators, transmission facilities, and loads in addition to the subject interconnection project in this study. Applicable seasonal conditions and the appropriate study years for the planning horizon are also incorporated. Additional assumptions are listed as follows.

1) The generation in the study area are dispatched to the patterns that stress the transmission system in the study area. In these patterns, the associated generators are typically set to their Maximum Power Outputs (MPO) unless otherwise specified.

2) The West Kelowna Transmission Project (WKTP) Alterative 3E[1] is included in the study model. WKTP will build a new 138 kV line from BC Hydro's West Bank substation (WBK) to Fortis BC's Recreation substation (REC). The considered in-service date for WKTP is November 2032.

3) For the purpose of performing this study, Nicola Substation Transformation Capacity Reinforcement project (i.e. addition of NIC T7) and 1L243 reconductoring is assumed already completed by the time the IC's generating project enters service.

[1] BC Hydro, West Kelowna Transmission Project, see details in https://www.bchydro.com/energy-in-bc/projects/wktp.html

5 System Studies and Results

5.1 Power Flow Study Results

Power flow studies were performed to evaluate whether the IC's generating project would cause any unacceptable system performance (e.g. equipment overloads, steady-state voltage violation and voltage instability) and to determine the system reinforcement requirement based on steady state performance analysis.

The study focuses on the base scenario — 32HW/33LS/33HS system conditions that include all the higher-queued generating projects in the region. These base cases were prepared based on factors such as load conditions, seasonal variation in ambient temperatures, and generation patterns that stress the transmission system.

In addition to the base scenario, an additional scenario is studied for the first year after the [redacted] enters service (30HS/30LS/30HW).

The studies are performed for system normal conditions and under critical system contingencies in the P1 and P2 events specified by NERC TPL-001-4. Study results are summarized below.

5.1.1 Thermal Overload Analysis

The study shows that the addition of [redacted] would not cause any new thermal overloads under system normal condition.

For critical N-1 contingency (P1 and P2 events) conditions, the study observed several pre-existing overloads on 138 kV circuits such as 1L203, 1L205, 1L244_A, 1L244_B and SVA T3. Those overloads will be addressed by planned generation shedding or runback RAS at [redacted]. The [redacted] marginally contributes to these overloads and may need to participate in the generation runback RAS, which will be determined during the System Impact Study (SIS) stage in future if needed.

The details of thermal overload analysis results can be found in Appendix B.

5.1.2 Steady-State Voltage Analysis

With the connection of the IC's project, the stead-state voltage performance under system normal and single contingency conditions is acceptable for two sets of study scenarios: the base study scenarios (33LS, 33HS, 32HW) and the sensitivity study scenarios (30LS, 30HS, 30HW). Appendix B shows the details in the steady-state voltage study results.

5.1.3 Reactive Power Capability Evaluation

The BC Hydro TIR requires IBR power plant to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range.

Based on the power flow model data submitted by the IC, the proposed [redacted] be capable of meeting the BC Hydro's reactive capability requirement at the plant's maximum MW output, which is subjected to further verification in the next stage of the interconnection process.

In addition, according to the reactive capability data provided by the IC, the proposed WTG would offer a reactive capability range of +2.8 Mvar to -2.8 Mvar at zero MW output, provided that the turbine's "Optional/Extended Range with Reactive Power at Standstill" function—outlined in the Generation Capability Curve plot from the *Generator Capability Curve (Wind).pdf*—is enabled. This function should be re-confirmed if the IC's project advances to the next stage of the interconnection process.

5.1.4 Anti-Islanding Requirements

[redacted] is not arranged for islanded operation. In addition, the IC is required to install anti-islanding protection within its facility to disconnect the IC's wind farm from the grid when an inadvertent island with the local loads forms.

5.1.5 Other Performance Requirements

Fast Frequency Response, per BC Hydro's TIR Section 6.4.5, is required at the [redacted] The proposed wind turbine generators, when equipped with the FFR function, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The FFR settings should be determined in coordination with BC Hydro in the later stage of the interconnection process.

5.2 Fault Analysis

The short circuit analysis in the FeS is based upon the latest BC Hydro system model, which includes the generating facility information and associated impedance data provided by the IC. A more detailed study will be performed at the system impact study stage if needed.

5.3 Stations Requirements

Nicola substation (NIC) will be upgraded to provide a 230 kV line termination to allow connection to the [redacted]

The station upgrade scope at the existing Nicola substation (NIC) is as follows.

- Add one 230 kV line position with associated substation equipment including one 230 kV circuit breaker, three manual disconnect switches, one motor-operated disconnect switch, one CT, one CVT, and one surge arrester. Appendix C shows the associated one-line diagrams for details.
- Upgrade required substation facilities, infrastructures, and bus work to support new station equipment.
- Terminate 230kV line of [redacted] at the station.
- Install associated P&C, station service and other associated equipment in the existing control building.
- The location of metering kits will be determined in next stage.
- Other associated station work.

6 Cost Estimate and Schedule

The non-binding good faith estimated cost and time to construct the Network Upgrades required to interconnect the proposed project will be provided in a separate letter to the IC.

7 Conclusions

To interconnect the [redacted] and its facilities to the BCH Transmission System at the POI, this Feasibility Study has identified the following conclusions and requirements:

1. A new 230 kV line position is required at NIC substation to facilitate the interconnection of [redacted].
2. The connection of [redacted] does not cause any performance violation (i.e. thermal overload, voltage performance violation or voltage stability concern) under system normal conditions.
3. Under critical single system contingency (N-1) conditions, the study has observed thermal overloads on 1L203, 1L205, 1L244_A, 1L244_B and SVA T3. The [redacted] may need to participate in the generation runback or shedding remedial action scheme (RAS) to maintain the system security. The RAS function scope will be specified in the System Impact Study (SIS) if the need for RAS is determined.
4. [redacted] is required to install anti-islanding protection within its facility to disconnect the IC's generating plant from the grid when an inadvertent island with the local load forms. The anti-islanding protection shall be configured in the manner that does not compromise the required fault ride-through performance.
5. The [redacted] is required to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range, per BC Hydro's TIR Section 6.4.2.
6. The "Extended Range with Reactive power at Standstill" for the proposed type 4 WTGs, as described in the Generation Capability Curve plot from Generator Capability Curve (Wind).pdf file, is required so that each turbine can provide reactive power capability at zero MW output. BC Hydro recognizes that Type-4 WTGs with the "Extended Range with Reactive power at Standstill" have an inherent limitation—providing only partial required reactive power capability during turbine standstill.

7. Fast Frequency Response is required at the [redacted]. The proposed wind turbine generators, when equipped with the FFR function, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The FFR settings should be determined in coordination with BC Hydro in the later stage of the interconnection process.

Appendix A
Schematic Diagram of the IC's Project

Figure A-1 shows the schematic diagram for the [redacted].

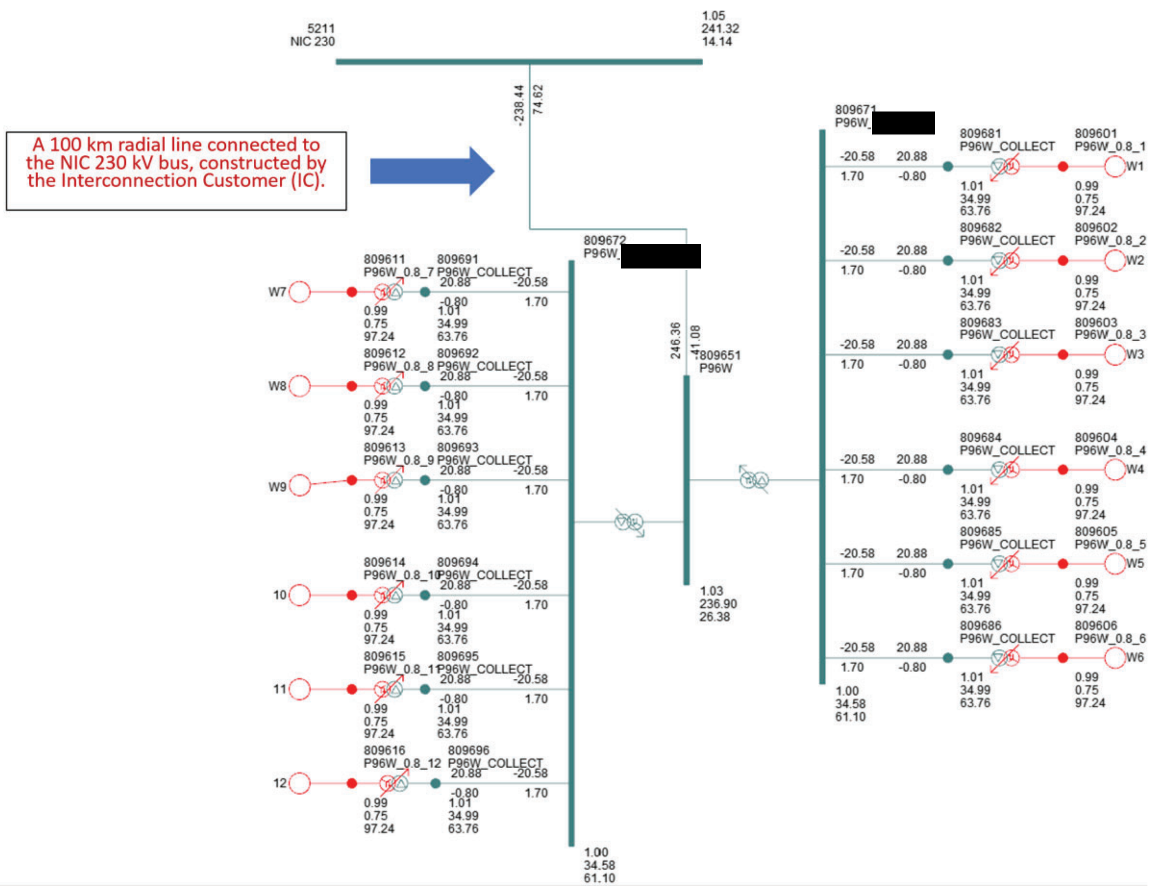

Figure A-1: [redacted] Plant Schematic Diagram.

Appendix B

Power Flow Study Results

Base Scenario (32HW/33HS/33LS)

Table B-1: Thermal Overload Study Results

Case	SIW Regional Genera-tions (Note 1)	Contingency		Branch Loading (% of its seasonal normal rating)								
				NIC T3	NIC T5	2L265	1L244_A (Note 1)	1L244_B (Note 2)	1L240_X (Note 3)	1L203	1L205	SVA T3
		Cat.	Description	-	-	NIC-VVW	NIC-[redacted]	[redacted] WBK	WBK-REC	HLD-SVA	HLD-SVA	-
Winter Rating in MVA				1425	287	318.7	251.9	219.9	173.1	191.2	149.6	178
32HW	Max	P0	System Normal	11.2	19.1	38.5	65.7	54.6	12.1	83.8	75.3	44.8
	Max	P1.2	1L203	10.3	19.6	47.9	65.6	54.8	12.3	0	**110.4**	26.5
	Max	P1.2	1L205	12.1	23.3	42.4	64.8	55.7	13.2	**118.5**	0	38.2
	Max	P1.2	1L244_A	6.2	2.4	36.5	0	**140.5**	**105.7**	80.5	71.4	42.8
	Max	P1.2	1L244_B	13.4	26.5	40.1	95.6	0	50	85.3	77.2	45
	Max	P1.2	1L251	14.1	28.5	39.2	63.6	57	14.5	85.8	77.8	47.2
	Max	P1.2	2L265	13.8	15.5	0	64.4	56.5	14.1	92.2	85.5	33.2
	Max	P1.2	5L87	6.4	12.5	55.3	66.4	53	11.9	99.6	94.2	88.3
	Max	P1.2	5L83	12	17.6	41.1	65.7	54.3	12.2	87.3	79.6	55.3
	Max	P1.3	SVA T1	12.4	21	33.1	65.3	55	12.6	78.5	69	59.7
	Max	P1.3	NIC T2 (+T6)	20.3	24.7	40.2	62.7	58.2	15.6	86	78	47.7
	Max	P2.1	Open 1L203 at SVA	12.4	25.4	45.6	64.3	56.3	13.8	0	**140.2**	34.8
	Max	P2.1	Open 1L243 at HLD	11.8	22	41.2	65.1	55.4	12.9	76.7	66.8	40.6
	Max	P2.1	Open 1L244_B at WBK	14.2	29.2	40.2	**106.6**	13.4**	50	85.8	77.8	45.7
	Max	P2.3	NIC 1CB19	25.7	37.6	41.2	59.5	61.9	19.7	88.9	81.6	51.5
	Max	P2.3	NIC 2CB11	26	18.8	0	60.8	60.8	18.5	95.3	89.3	35.5
Summer Rating				1200	287	318.7	229.7	169.7	173.1	172.8	118.6	150
33HS	Max	P0	System Normal	14.4	19.8	36.9	70.6	64.1*	10.9	92.8	96.4	57.1
	Max	P1.2	1L203	13.4	20.4	45.7	70.4	64.3*	11.1	0	**142.1**	36.1
	Max	P1.2	1L205	15.4	24	40.3	69.6	65.3*	11.8	**131.6**	0	49.2
	Max	P1.2	1L244_A	8.6	3.7	35.3	0	**158.8***	**103.4**	89.2	91.5	54.6
	Max	P1.2	1L244_B	17.1	27.3	38.3	**104.7**	0	61	94.6	98.9	57.3
	Max	P1.2	1L251	17.8	29.1	37.3	68.4	66.7*	12.8	95	99.4	59.8
	Max	P1.2	2L265	16.9	16.7	0	69.4	66.1*	12	**100.4**	**106.8**	45.6
	Max	P1.2	5L87	9.9	14.3	51.1	71.6	62.6*	9.1	**107.5**	**116.4**	**100.2**
	Max	P1.2	5L83	14	19.3	39	71.3	64*	10.5	95.7	**100.4**	65.9
	Max	P1.3	SVA T1	15.9	21.8	31.9	70.2	64.6*	11.2	86.7	88	75.5
	Max	P1.3	NIC T2 (+T6)	26.2	25.8	38.2	67.2	68.2*	14.4	95.4	**100**	60.7
	Max	P2.1	Open 1L203 at SVA	15.8	26.1	43.7	69.1	65.9*	12.3	0	**178.6**	44.7
	Max	P2.1	Open 1L243 at HLD	14.9	21.6	38.4	70.2	64.6*	11.3	87.9	89.8	54.1
	Max	P2.1	Open 1L244_B at WBK	18.1	30	38.4	**116.8**	17.3**	61	95.2	99.7	58.1

	Max	P2.3	NIC 1CB19	33	38.9	38.8	64.1	72.6*	17.9	98.6	**104.2**	64.5
	Max	P2.3	NIC 2CB11	31.9	20.6	0	65.4	70.9*	16.4	**104**	**111.6**	48.6
Summer Rating				1200	287	318.7	252.6	229.1	173.1	172.8	118.6	150
33LS	Max	P0	System Normal	20.6	28.4	7	82.7	46.9*	19.2	89.7	91.2	65.3
	Max	P1.2	1L203	19.4	28.8	16.1	82.7	47*	19.4	0	**133.5**	44.2
	Max	P1.2	1L205	21.6	32.4	10.7	81.8	48*	20.4	**126.7**	0	57.7
	Max	P1.2	1L244_A	13.6	9.4	5.6	0	**158.6***	**129**	85.5	85.5	62.5
	Max	P1.2	1L244_B	22.4	33.4	8	**104.6**	0	27.2	90.8	92.8	65.3
	Max	P1.2	1L251	23.8	36.9	7.4	80.7	49.3*	21.6	91.7	93.9	67.7
	Max	P1.2	2L265	21.3	27.8	0	82.5	47.3*	19.6	91.3	93.4	62.4
	Max	P1.2	5L87	17.5	24.9	18.5	83.9	45.9*	18.3	**101.3**	**106.9**	**100.3**
	Max	P1.2	5L83	20.1	27.8	8.7	82.9	46.7*	19.1	92.4	94.9	73.5
	Max	P1.3	SVA T1	22.5	30.7	3.6	82.2	47.5*	19.8	92.7	81.5	86.5
	Max	P1.3	NIC T2 (+T6)	37.9	37	10.3	77.7	53.4*	25.6	93.6	96.5	70.9
	Max	P2.1	Open 1L203 at SVA	22	34.6	13.6	81.3	48.7*	21	0	**170.6**	54
	Max	P2.1	Open 1L243 at HLD	20	26.1	5.5	83.3	46.2*	18.6	97	**101.2**	69.3
	Max	P2.1	Open 1L244_B at WBK	23.4	36	8.1	**116.6**	17**	27.2	91.5	93.6	66.1
	Max	P2.3	NIC 1CB19	44.1	49.1	11.9	74.9	57.1*	29.3	96.4	**100.3**	74.8
	Max	P2.3	NIC 2CB11	39.9	35.4	0	77.1	54.1*	26.4	96.2	**100.1**	66.5

Note 1: 1L244_A assumed uprated to a summer continuous rating of 961A or higher after [redacted] and [redacted] enters service.

Note 2: by default, the line loading on 1L244_B is measured at WBK end, except:

- If marked with asterisk "*", the line loading is measured on Section from PSW tap to BDM tap.
- If marked with double asterisk "**", the line loading is measured on Section from [redacted] to PSW tap.

Note 3: The BCH-FBC new tie line (WBK-REC) is assumed to have a summer continuous rating of 173.1 MVA, and its winter rating is not yet available yet. The summer rating is used as a placeholder in winter cases.

Table B-2: Steady-State Voltage Study Results

Case	IC's Plant Output	Contingency		Bus Voltage (PU)			
		Cat.	Description	NIC 230	NIC 138	VVW 230	P96W
32HW	Max	P0	System Normal	1.04	1.02	1.02	1.03
	Max	P1.2	2L265	1.04	1.06	N/A *	1.03
	Max	P1.2	5L87	1.01	1.01	0.99	1.03
	Max	P1.3	NIC T2 (+T6)	1.04	1.02	1.01	1.03
	Max	P2.3	NIC 2CB11	1.04	1.02	N/A *	1.03
33HS	Max	P0	System Normal	1.05	1.02	1.01	1.03
	Max	P1.2	2L265	1.05	1.02	N/A *	1.03
	Max	P1.2	5L87	1.03	1.02	1.00	1.03
	Max	P1.3	NIC T2 (+T6)	1.04	1.01	1.01	1.03
	Max	P2.3	NIC 2CB11	1.04	1.02	N/A *	1.03
33LS	Max	P0	System Normal	1.05	1.02	1.05	1.03
	Max	P1.2	2L265	1.05	1.02	N/A *	1.03
	Max	P1.2	5L87	1.04	1.02	1.04	1.03
	Max	P1.3	NIC T2 (+T6)	1.04	1.01	1.04	1.03
	Max	P2.3	NIC 2CB11	1.05	1.02	N/A *	1.03

Note *: VVW T2 and T3 will be isolated after 2L265 fault is cleared. The VVW 230 bus will be isolated.

Additional Scenario (30HW/30HS/30LS)

Table B-3: Thermal Overload Study Results

Case	SIW Regional Genera-tions (Note 1)	Contingency		Branch Loading (% of its seasonal normal rating)							
				NIC T3	NIC T5	2L265	1L244_A (Note 1)	1L244_B (Note 2)	1L203	1L205	SVA T3
		Cat.	Description	-	-	NIC-VVW	NIC-[redacted]	[redacted] WBK	HLD-SVA	HLD-SVA	-
Winter Rating in MVA				1425	287	318.7	251.9	219.9	172.8	149.6	178
30HW	Max	P0	System Normal	6.7	5.6	38.8	15.7	43.3	80.8	71.8	40.9
	Max	P1.2	1L203	5.9	5.8	48	15.8	43.3	0	**104.9**	23.1
	Max	P1.2	1L205	7.6	9.7	42.4	15.6	43.3	**113.9**	0	34.6
	Max	P1.2	1L244_A	5.8	2.2	38.6	0	0	80.1	71	40.2
	Max	P1.2	1L244_B	8.4	11	38.8	40.9	0	82.1	73.3	42.4
	Max	P1.2	1L251	9.8	15.5	39	15.6	43.3	82.9	74.3	43.3
	Max	P1.2	2L265	9.4	2.4	0	15.9	43.3	89.4	82.1	28.8
	Max	P1.2	5L87	2.5	2.6	56	15.6	43.3	96.9	91	85.2
	Max	P1.2	5L83	5.9	4.4	39.7	16.2	43.3	84.5	76.2	51.4
	Max	P1.3	SVA T1	7.8	7.4	33.8	15.7	43.3	76.1	66.1	54.9
	Max	P1.3	NIC T2 (+T6)	12.5	7.8	39.5	15.6	43.3	82.1	73.3	42.9
	Max	P2.1	Open 1L203 at SVA	7.9	11.9	45.3	15.6	43.3	54.7	**134.9**	31.8
	Max	P2.1	Open 1L243 at HLD	7.2	7.8	40.7	15.7	43.3	76	66	37.9
	Max	P2.1	Open 1L244_B at WBK	9.2	13.8	38.9	**53.7**	13.4**	82.6	73.9	42.9
	Max	P2.3	NIC 1CB19	18.2	21.1	40.6	15.8	43.3	85	76.8	46
	Max	P2.3	NIC 2CB11	18.3	3	0	15.7	43.3	91.3	84.4	30.2
Summer Rating				1200	287	318.7	169.7	169.7	172.8	118.6	150
30HS	Max	P0	System Normal	6.8	5.6	35.1	18.5	62.4*	88.9	90.8	50
	Max	P1.2	1L203	8.0	5.8	44.6	17.8	61.7*	0	**134.3**	30
	Max	P1.2	1L205	9.9	9.6	39.2	17.7	61.8*	**126.6**	0	44
	Max	P1.2	1L244_A	8	3.2	35.7	0	0	89	91.1	51
	Max	P1.2	1L244_B	11.1	12.1	36.2	53.1	0	91.1	94	53.6
	Max	P1.2	1L251	12.6	15.4	36.4	17.7	62*	91.9	95	54.8
	Max	P1.2	2L265	11.5	2.8	0	18.2	61.5*	97.6	**103**	44.6
	Max	P1.2	5L87	3.7	2.1	49.6	17.4	62.2*	**104.7**	**112.6**	97.3
	Max	P1.2	5L83	7.4	4.2	36.6	17.7	61.9*	92.2	95.4	59
	Max	P1.3	SVA T1	10.2	7.3	30.7	17.7	61.8*	83.9	84.1	68.8
	Max	P1.3	NIC T2 (+T6)	16.3	6.8	36.5	17.7	62*	90.8	93.5	53.6
	Max	P2.1	Open 1L203 at SVA	10.3	11.8	42.3	17.7	61.9*	0	**171.4**	40.2
	Max	P2.1	Open 1L243 at HLD	9.2	6.4	36.6	17.8	61.7*	87	88.3	49.9
	Max	P2.1	Open 1L244_B at WBK	12.1	14.9	36.4	69.7	17.1**	91.8	94.9	54.4
	Max	P2.3	NIC 1CB19	23.8	21.3	37.2	17.7	61.8*	94.3	98.4	58.6
	Max	P2.3	NIC 2CB11	22.2	2.4	0	17.8	61.7*	99.8	**105.9**	46.2
Summer Rating				1200	287	318.7	169.7	169.7	172.8	118.6	150
30LS	Max	P0	System Normal	15.4	16.2	10.9	42.4	26.9*	87.4	87.8	58.9
	Max	P1.2	1L203	14.2	16.4	18.8	42.4	26.9*	0	**127.7**	38.3
	Max	P1.2	1L205	16.4	20.1	13.7	42.4	26.9*	**122.9**	0	51.7
	Max	P1.2	1L244_A	12.7	9.1	10.6	0	0	85.8	85.5	56.8

	Max	P1.2	1L244_B	16	17.9	11	52.5	0	87.8	88.4	59.4
	Max	P1.2	1L251	19.1	25.3	10.9	42.7	26.9*	89.6	90.8	62.2
	Max	P1.2	2L265	16.2	15.6	0	42.4	26.9*	89.6	90.8	56.1
	Max	P1.2	5L87	12.4	12.8	18.7	42.4	26.9*	97.3	**101.4**	89.5
	Max	P1.2	5L83	15.2	15.8	11.4	43.1	26.9*	89.3	90.4	65.1
	Max	P1.3	SVA T1	17.1	18.4	7.6	42.4	26.9*	81	79	78.1
	Max	P1.3	NIC T2 (+T6)	29.3	22	12.5	42.7	26.9*	90.3	91.7	63.2
	Max	P2.1	Open 1L203 at SVA	17	22.5	16.6	42.8	26.9*	0	**164.8**	47
	Max	P2.1	Open 1L243 at HLD	14.5	13.2	9.4	42.4	26.9*	96.8	**100.7**	64.2
	Max	P2.1	Open 1L244_B at WBK	17.4	20.9	11	69.7	17.8**	88.6	89.5	60.9
	Max	P2.3	NIC 1CB19	35.8	34.3	13.4	42.4	26.9*	93.4	96.1	67.6
	Max	P2.3	NIC 2CB11	31.4	20.7	0	42.4	26.9*	93.4	96	59.1

Note 1: 1L244_A assumed uprated to a summer continuous rating of 961A or higher after [redacted] and [redacted] enters service.

Note 2: by default, the line loading on 1L244_B is measured at WBK end, except:

- If marked with asterisk "*", the line loading is measured on Section from PSW tap to BDM tap.
- If marked with double asterisk "**", the line loading is measured on Section from [redacted] to PSW tap.

Table B-4: Steady-State Voltage Study Results

Case	IC's Plant Output	Contingency		Bus Voltage (PU)			
		Cat.	Description	NIC 230	NIC 138	VVW 230	P96W
30HW	Max	P0	System Normal	1.05	1.02	1.02	1.03
	Max	P1.2	2L265	1.05	1.02	N/A *	1.03
	Max	P1.2	5L87	1.01	1.02	0.99	1.03
	Max	P1.3	NIC T2 (+T6)	1.04	1.02	1.02	1.03
	Max	P2.3	NIC 2CB11	1.04	1.02	N/A *	1.03
30HS	Max	P0	System Normal	1.05	1.02	1.02	1.03
	Max	P1.2	2L265	1.05	1.02	N/A *	1.03
	Max	P1.2	5L87	1.01	1.01	0.98	1.03
	Max	P1.3	NIC T2 (+T6)	1.04	1.02	1.01	1.03
	Max	P2.3	NIC 2CB11	1.05	1.02	N/A *	1.03
30LS	Max	P0	System Normal	1.05	1.01	1.04	1.03
	Max	P1.2	2L265	1.05	1.01	N/A *	1.03
	Max	P1.2	5L87	1.04	1.01	1.03	1.03
	Max	P1.3	NIC T2 (+T6)	1.04	1.02	1.03	1.03
	Max	P2.3	NIC 2CB11	1.05	1.01	N/A *	1.03

Note *: VVW T2 and T3 will be isolated after 2L265 fault is cleared. The VVW 230 bus will be isolated.

Appendix C
One-Line Sketch for Nicola Substation Upgrade

Figure C-1 illustrates the Stations planning One-Line Sketch for the Nicola substation upgrade. This diagram highlights only the portions of the Nicola substation that affected by the proposed interconnection of [redacted].

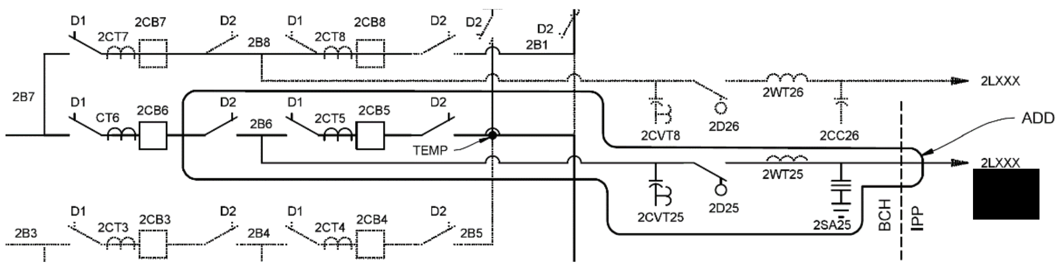

Figure C-1: Stations Planning One-Line Sketch for the Nicola substation upgrade.