BC Hydro
Power smart

6911 Southpoint Drive (B03)
Burnaby, BC
V3N 4X8

November 24, 2025

[redacted]

via email: [redacted]

RE: CEAP IR #13 – [redacted] – Interconnection Feasibility Study

Dear [redacted]

Enclosed is the Interconnection Feasibility Study for the proposed Interconnection Request (IR), [redacted], submitted under Attachment M-2: Transmission Service and Interconnection Service Procedures for Competitive Electricity Acquisition Process (CEAP) of the Open Access Transmission Tariff (OATT). This letter provides a non-binding good faith estimate of the cost and time to construct the facilities required to interconnect your project to BC Hydro's Transmission System, being the Network Upgrades, based on the findings of the Interconnection Feasibility Study.

Open Access Transmission Tariff

The OATT defines Network Upgrades as additions, modifications, and upgrades to BC Hydro's Transmission System required at or beyond the Point of Interconnection to accommodate the interconnection of the Generating Facility to the BC Hydro's Transmission System. Pursuant to the OATT, BC Hydro will design, procure, construct, install, and own the Network Upgrades. While BC Hydro will pay the costs for the Network Upgrades, the Interconnection Customer provides security for such costs.

Interconnection Study Costs

The Interconnection Customer is responsible for paying the full cost of all Interconnection Studies in cash. Interconnection Study costs vary depending on the scope, complexity, and other factors such as whether any scope is shared with another Interconnection Customer (not applicable to this Interconnection Feasibility Study). The deposit amounts specified in the OATT are not proxy Interconnection Study costs. If actual Interconnection Study costs exceed the deposit amount, the Interconnection Customer must pay the remaining balance in cash. Please refer to the answer for question no. 53 in the posted Questions & Answers for 2025 Call for Power for typical study cost ranges.

Cost Estimate

Based on the Interconnection Feasibility Study, the non-binding good faith estimated cost (typical accuracy range of +150%/-50%) for Network Upgrades required to interconnect your project is $24.5 M.

Major Scope of Work Identified:

- Add one 230 kV line position with a circuit breaker and disconnects to form a 4 breaker ring bus at BC Hydro's Meikle Terminal station (MKT)
- Add one-line terminal including a motor-operated disconnect switch, surge arrester and capacitor voltage transformer and terminate the Interconnection Customer's transmission line at MKT

- Upgrade required substation facilities, infrastructures, and bus work to support new station equipment
- Supply and install required Protection, Control and Telecommunications equipment

Exclusions:

- GST
- Permits
- Right-of-Way & property costs

Key Assumptions:

- Construction by contractor
- 8 months of construction is considered
- No construction during winter season
- Execution of early Engineering and Procurement Agreement
- No expansion of existing stations or control buildings to accommodate new equipment
- Impact Benefit Agreements with First Nations are not considered

Key Risks:

- Expansion of the existing control building may be required leading to increased costs and/or a longer project schedule
- Major equipment delivery presents potential project cost and schedule risks, based on variance in equipment lead times
- No defined supply chain strategy; construction costs may increase depending on delivery method
- Project schedule may be longer than expected, leading to increased overhead costs
- Ground improvements may be required leading to increased construction costs
- Contaminated soil may be encountered leading to increased construction costs
- Cost of materials and major equipment may be affected by market conditions and escalation

Study Limitations and Exclusions

Protection, Control, and Telecommunications

The Interconnection Feasibility Study does not include a detailed review of the protection, control, and telecommunications system requirements specific to your Interconnection Request. Based on a high-level review, we have identified proxy costs for protection, control, and telecom Network Upgrades drawn from comparable interconnection projects with similar scope and complexity; these proxy costs have been included solely for indicative budgeting purposes. The relative interconnection cost determined by the Interconnection Feasibility Study includes a telecommunications component based on an assumed solution to deliver teleprotection and telecontrol circuit requirements necessary for the Interconnection Request. Protection, control, and telecommunications system requirements will be reviewed in detail in the System Impact Study if you are a successful participant of the CEAP and meet applicable requirements.

For Interconnection Feasibility Study purposes, it is assumed that any applicant-proposed works that could obstruct or impair the performance of existing BC Hydro microwave systems or new links from the proposed Interconnection Customer Interconnection Facilities (ICIF) to the BC Hydro microwave system would be identified and either relocated or repositioned as determined in a System Impact Study if you are a

successful participant of the CEAP and meet applicable requirements. Such works may include, but are not limited to, towers, turbines, dams, support structures, panels, surface materials deposited or redistributed, water surface changes, or vegetation.

Generation Shedding/Curtailment Scheme and Electromagnetic Transient (EMT) Studies

The generation shedding/curtailment scheme reviews (e.g., Remedial Action Scheme (RAS), and a direct transfer trip for anti-islanding scheme) and EMT studies are completed in a System Impact Study. The outcomes of these studies may result in additional requirements, which could include Network Upgrades or ICIF. Any costs associated with completion of these studies, and resulting requirements, are not included in the Interconnection Feasibility Study cost estimate.

Revenue Metering

Please note that revenue metering requirements have not been determined with the Interconnection Feasibility Study. As such, any costs associated with revenue metering and other interconnection components are not included in the cost estimate provided above. Once these requirements are defined, costs that are attributable to the Interconnection Customer are to be paid in cash. For more details on revenue metering requirements and responsibilities, please refer to:

https://www.bchydro.com/content/dam/BCHydro/customer-portal/documents/distribution/standards/ds-rmr-complex-revenue-metering.pdf.

Schedule

Based on the Interconnection Feasibility Study, the non-binding good faith estimated in-service date for your Interconnection Request's Network Upgrades is Quarter 3 2031 (calendar year). To achieve this timeline, we may need to expedite certain activities, including engineering design and procurement of long-lead equipment.

Timely actions required from you to minimize risks to the schedule:

- Submission of additional technical data required for the System Impact Study and Facilities Study
- Submission of any required information or document such as demonstration of Site Control
- Execution of Combined Study Agreement and Standard Generator Interconnection Agreement
- Financial commitments and securities

Please note that changes to your Interconnection Request or delays in data submission or financial commitments may also impact the target in-service date.

If you have any questions, please contact the BC Hydro CEAP team at ceap2025@bchydro.com.

Sincerely,

[redacted]

[redacted]

Manager, Customer Interconnections

BC Hydro

Encl.: CEAP_2025_IR13_[redacted]_Feasibility_Study.pdf

BC Hydro
Power smart

[redacted]

Interconnection Feasibility Study

BC Hydro EGBC Permit to Practice No: 1002449

2025 CEAP IR # 13

Prepared for: [redacted]

Prepared by: [redacted] [redacted]

Engineer, Transmission Operations Services

Reviewed by: [redacted]

Principal Engineer, Transmission Operations Services

Accepted by: [redacted]

Manager, Transmission Planning

Report Metadata

Header:	2025 CEAP IR # 13
Subheader:	Interconnection Feasibility Study
Title:	[redacted]
Subtitle:	2025 CEAP IR # 13
Report Number:	1000-APR-00046
Revision:	0
Confidentiality:	Public
Date:	2025 Nov 21
Volume:	1 of 1
Prepared for:	[redacted]
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Reviewed by:	[redacted]
Title:	Principal Engineer, Transmission Operations Services
Related Facilities:	MKT – Meikle Terminal Station
Additional Metadata:	Transmission Planning 2025-054 Filing Subcode 1350

Revisions

Revision	Date	Description
0	2025 Nov	Initial release

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Entire report except listed below	Transmission Operations Services

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Engineer, Transmission Operations Services

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Section:	**Discipline:**
5.2, 5.3	Stations Planning

Contributed by:

[redacted]

Specialist Engineer, Station Planning

[redacted]

Executive Summary

[redacted]c., the interconnection customer (IC), requests to interconnect its [redacted] (2025 CEAP IR # 13) to the BC Hydro (BCH) system. [redacted] has seventeen (17) [redacted] type-3 wind turbine generators with total installed capacity of 100.3 MW. The proposed Point of Interconnection (POI) is at BC Hydro's 230kV Meikle Terminal Station (MKT). The IC's project will connect to the POI via 22.3 km 230 kV customer-owned transmission line. The IC's proposed commercial operation date (COD) is Feb 5th, 2031.

To interconnect the [redacted] and its facilities to the BCH Transmission System at the proposed POI, this Feasibility Study has made the recommendations and conclusions as follow:

1. A new 230 kV line position is required at Meikle Terminal Station (MKT) to facilitate the interconnection of [redacted]
2. The connection of [redacted] does not cause any performance violation (i.e. thermal overload, voltage performance violation or voltage stability concern) under system normal conditions.
3. The connection of [redacted] will exacerbate the pre-existing thermal overload on the BC Hydro lines 2L308 and 2L312 and introduce a new overload on 2L309 under single contingencies or breaker contingencies. The [redacted] will be required to participate in the existing Peace Region Local Gen Shed RAS. The IC is also required to participate in GMS Area Gen Shed RAS for Peace 500 kV transmission line contingencies. Detailed Peace Region Local Gen Shed RAS and GMS Area Gen Shed RAS functional requirements modifications will be specified later if the IC's project proceeds to next stage of the interconnection process.
4. [redacted] is required to install anti-islanding protection within its facility to disconnect the IC's generating plant from the grid when an inadvertent island with the local load forms. The anti-islanding protection shall be configured in the manner that does not compromise the required ride-through performance.

5. [redacted] is required to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range, per BC Hydro's TIR Section 6.4.2.

6. The "STATCOM option" for the proposed type-3 WTGs is required so that each turbine can provide reactive power capability at zero MW output. BC Hydro recognizes that Type-3 WTGs with the STATCOM option have an inherent limitation—providing only partial reactive power capability during turbine standstill.

7. Fast Frequency Response, also known as Virtual Inertia Control (VIC) in the proposed wind turbines is required at [redacted] The proposed wind turbine generators, when equipped with the VIC option, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The VIC settings should be determined in coordination with BC Hydro in the later stage of the interconnection process.

The above conclusions are made based on the IC's input data and study assumptions listed in Section 4, which represent the best available information on October 14, 2025.

A non-binding good faith cost for required network upgrades and estimated schedule for construction are included in a separate letter to the IC.

Please note that, this Feasibility Study report does not include the descriptions of Protection, Control, and Telecommunications requirements and the associated upgrade scopes; however, as discussed in Section 2 "Purpose and Scopes of Study, the associated cost implications are captured and delivered in the cover letter to the IC".

Contents

Appendices

Acronyms

The following are acronyms used in this report.

BCH	BC Hydro
CEAP	Competitive Electricity Acquisition Process
COD	Commercial Operation Date
ERIS	Energy Resource Interconnection Service
FeS	Feasibility Study
GMS	Gordon M. Shrum Generating Station
IBR	Inverter-Based Resources
IC	Interconnection Customer
IR	Interconnection Request
MPO	Maximum Power Output
NERC	North American Electric Reliability Corporation
NRIS	Network Resource Interconnection Service
OATT	Open Access Transmission Tariff
POI	Point of Interconnection
RAS	Remedial Action Scheme
TIR	BC Hydro “60 kV to 500 kV Technical Interconnection Requirements for Power Generators”
WECC	Western Electricity Coordinating Council
WTG	Wind Turbine Generator

1 Introduction

Table 1-1 below summarizes the project reviewed in this Feasibility Study.

Table 1-1 Summary of Project Information

Project Name	[redacted]	
Name of Interconnection Customer (IC)	[redacted]	
Point of Interconnection (POI)	Meikle Terminal Station (MKT)	
IC's Proposed COD	5th February 2031	
Type of Interconnection Service	NRIS ☒	ERIS ☐
Maximum Power Injection (MW)	98.34 MW (Summer)	98.34 MW (Winter)
Number of Turbines	17 x 5.9 MW	
Plant Fuel	Wind	

[redacted] the interconnection customer (IC), requests to interconnect its [redacted] (2025 CEAP IR # 13) to the BC Hydro system. [redacted] has seventeen (17) [redacted] type-3 wind turbine generators with total installed capacity of 100.3 MW. The IC's proposed Point of Interconnection (POI) is at BC Hydro's 230kV Meikle Terminal Station (MKT). The IC's project will connect to the POI via 22.3 km 230 kV customer-owned transmission line. The proposed commercial operation date (COD) is Feb 5th, 2031.

Figure 1-1 shows the Peace Region 138/230/500kV transmission system diagram. The Peace Regional System is connected to BC Hydro 500kV Bulk System through two 500kV substations GMS and SBK:

- One 230 kV transmission line 2L308 and two 138 kV transmission lines 1L361 and 1L364 connecting GMS substation to Peace Regional system, and
- Two 230 kV transmission lines 2L391 and 2L392 and two 138 kV transmission lines 1L360 and 1L374 connecting SBK substation to Peace Regional system.
- There are two 500 kV transmission lines 5L5 and 5L6 connecting SBK to PCN 500 kV substation, and through eight 500 kV transmission lines from GMS/PCN further down to BC Hydro load centre in the south.

[redacted] project is expected to connect to BC Hydro's 230 kV substation at Meikle Terminal Station (MKT), as shown in Figure 1.1 below. The Peace region 138/230 kV system has pre-existing branch overloading concerns under single or multiple contingencies, which are presently addressed by the existing Peace Region Generator Shedding RAS.

There is a higher-queued new wind farm project [redacted] with installed capacity of 54.6 MW, to be connected to BC Hydro Sukunka substation as shown on Figure 1-1. The projected in-service date for [redacted] is September 30, 2030.

In addition, there are two wind farm projects, which are also shown in Figure 1-1 below. Details about these two wind farms are as the following:

- [redacted] – 194 MW, tap connection on 2L391 at 28 km from SBK. In service date is October 1st, 2030.
- [redacted] – 195.9 MW, a three-circuit breaker ring switching station loop in and out of 2L392 at 22 km from SBK. The in-service date is September 30th, 2031.

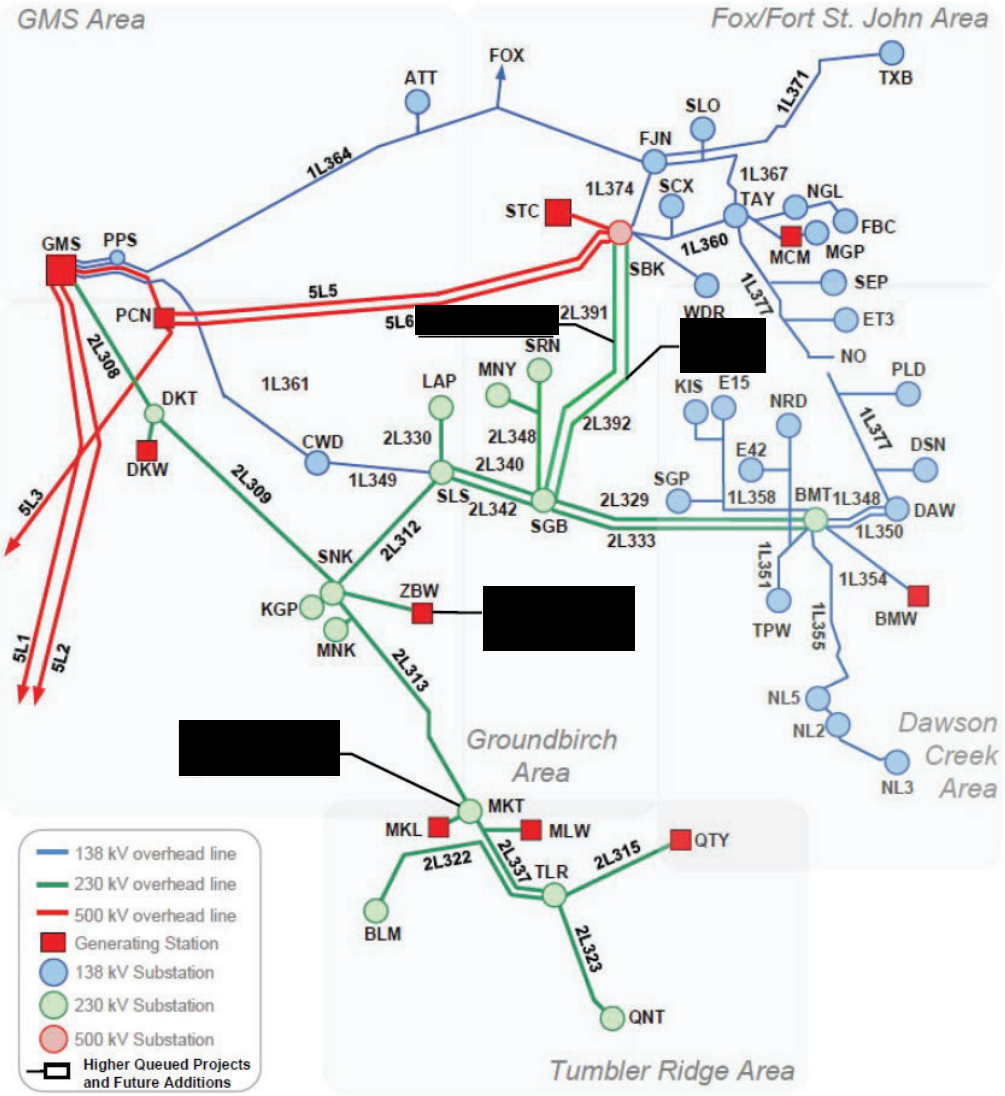

Figure 1-1: Peace Region 138/230/500 kV Transmission System Diagram

2 Purpose and Scopes of Study

This Feasibility Study is a preliminary evaluation of the system impact of interconnecting the proposed project to the BC Hydro system based on power flow and short circuit analysis in accordance with BCH's Open Access Transmission Tariff (OATT) and produces the estimated cost of required Network Upgrades and the implementation schedule.

Per OATT, the Feasibility Study is performed individually for each of the participating projects in the CEAP process and focuses specifically on the BC Hydro regional transmission system where the proposed generating project is connected and affects.

This is a "limited scope" study which is restricted to power flow studies of P0, P1 and P2 planning events as defined in TPL-001-4 and short circuit analysis. The study does not address other technical aspects such as transient stability and switching transients and impact of multiple contingencies. These subjects will be addressed in subsequent System Impact Study if the project proceeds further. In addition, any potential impacts to the adjacent external systems to BC Hydro would be addressed in subsequent detailed and coordinated studies with the relevant adjacent entities if the proposed generator project proceeds further.

Please note that, due to the compressed study timeline for 2025 CEAP Feasibility Study, this report does not include the descriptions of the Protection, Control, and Telecommunication requirements and the associated upgrade scopes. Instead, the network upgrades associated with Protections, Controls and Telecommunications are incorporated with cost estimates in a separate cover letter to the IC.

3 Standard and Criteria

The Feasibility Study is performed in compliance with the North American Electric Reliability Corporation (NERC) and Western Electricity Coordinating Council (WECC) reliability standards, and the BCH interconnection requirements in the TIR, and upon the ratings of the existing BCH transmission facilities described in Operating Orders, specifically:

- NERC standards: TPL-001-4 and FAC-002-3 relevant to the scope of this Feasibility Study.
- WECC criteria TPL-001-WECC-CRT-4 Transmission System Planning Performance, July 1, 2023.
- BC Hydro's 60 kV to 500 kV Technical Interconnection Requirements for Power Generators, Rev 2.1.1, Effective: Sept 22, 2025.
- BC Hydro Operating Order 5T-10, Ratings for All Transmission Circuits 60 kV or Higher, Sept 17, 2025.
- BC Hydro Operating Order 5T-14, Ratings for All Transmission and Distribution Transformer, Sept 22, 2025.
- BC Hydro System Operating Order 7T-22 System Voltage Control, Sept 19, 2023.

4 Assumptions and Conditions

This Feasibility Study is performed based on the IC's submitted data and information available to BC Hydro on Oct 14, 2025, for the study purpose. Assumptions are made wherever the IC's input is unavailable. Appendix A shows the schematic diagram of the IC's project used in the study model.

The power flow study cases used in this Feasibility Study are established based upon the BC Hydro's base resource plan and load forecasts available at the time of performing the study, which includes existing and future generators, transmission facilities, and loads in addition to the subject interconnection project in this study. Applicable seasonal conditions and the appropriate study years for the study planning horizon are also incorporated. Additional assumptions are listed as follows.

1) The generation in the study area are dispatched to the patterns that stress the transmission system in the study area. In these patterns, the associated generators are typically set to their Maximum Power Outputs (MPO) unless otherwise specified.

2) The study includes following higher-queued wind farm projects that are planned within the Peace Region system:

   - [redacted] tap connection on 2L391 at 28 km from SBK. The projected in-service date is October 1, 2030.
   - [redacted] a three-circuit breaker ring switching station loop in and out of 2L392 at 22 km from SBK. The projected in-service date is September 30, 2031.
   - [redacted] connecting to Sukunka (SNK) substation. The projected in-service date is September 30, 2030.

3) BMT T4 300 MVA has planned to be in service by March 2027

4) A new 138 kV transmission line from SBK to TAY - 1L370 has been planned to be in service by March 2029.

5 System Studies and Results

5.1 Power Flow Study Results

Power flow studies were performed to evaluate whether the IC's generating project would cause any unacceptable system performance (e.g. equipment overloads, steady-state voltage violation and voltage instability) and to determine the system reinforcement requirement based on steady state performance analysis.

The study focuses on the base scenario — 2031 heavy winter (31HW), 2032 heavy summer (32HS), and 2032 light summer (32LS) system conditions that include the higher-queued generating projects ([redacted]) in the region. These base cases were prepared based on factors such as load conditions, seasonal variation in ambient temperatures, and generation patterns that stress the transmission system.

The studies are performed for system normal conditions and under critical system contingencies specified in the P1 and P2 events by NERC TPL-001-4. Study results are summarized below.

5.1.1 Thermal Overload Analysis

For all the studied load conditions (31HW/32HS/32LS), there is no branch overload identified under system normal condition (P0).

In the heavy / light summer load conditions (32HS, 32LS), the study has observed pre-existing branch overloads on BC Hydro's 230kV line 2L308 and 2L312 under single or multiple contingencies (i.e. 2L308 overlorded for loss of 2L312, or 2L312 overloaded for loss of 2L308). These overloads are presently addressed by the existing Peace Regin Generator Shedding remedial action scheme (RAS).

The connection of [redacted] will aggravate the pre-existing thermal overload on the BC Hydro lines 2L308 and 2L312 and introduce a new overload on 2L309 under single contingencies or breaker contingencies. See Appendix B (Table B-1) for branch loading study results. The existing Peace Region Local Gen-shedding RAS will continue to be relied upon to mitigate these overloads, and [redacted] is required to participate in the existing Peace Region Local Gen Shed RAS.

In addition to secure the Peace to Kelly Lake bulk transmission system under various operating conditions, [redacted] is required to participate in GMS Area Gen Shed RAS for Peace 500 kV transmission line contingencies.

Detailed Peace Region Local Gen Shed RAS and GMS Area Gen Shed RAS functional requirements modifications will be specified later if the IC's project proceeds to the next stage of the interconnection process.

5.1.2 Steady-State Voltage Analysis

With the connection of the IC's project, the stead-state voltage performance under system normal (P0) and single contingency conditions is acceptable for all the three load conditions (31HW, 32HS, 32LS). See Appendix B (Table B-2) for steady-state voltage study results.

5.1.3 Reactive Power Capability Evaluation

The BC Hydro TIR requires IBR power plant to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range.

Based on the power flow model data submitted by the IC, the proposed [redacted] would be capable of meeting the BC Hydro's reactive capability requirement at the plant's maximum MW output, which is subjected to further verification in the next stage of the interconnection process.

In addition, according to the IC-provided reactive capability data, the proposed WTG would provide total +28.9 Mvar to -32.3 Mvar reactive capability at the zero MW output if the turbine's "STATCOM" function is enabled. This function needs to be re-confirmed if the IC's project proceeds to next stage of the interconnection process.

5.1.4 Anti-Islanding Requirements

[redacted] is not arranged for islanded operation. In addition, the IC is required to install anti-islanding protection within its facility to disconnect the IC's wind farm from the grid when an inadvertent island with the local load forms.

5.1.5 Other Performance Requirements

Fast Frequency Response, also known as Virtual Inertia Control (VIC) in the proposed wind turbines is required at the [redacted]. The proposed wind turbine generators, when equipped with the VIC option, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The VIC settings should be determined in coordination with BC Hydro in the later stage of the interconnection process.

5.2 Fault Analysis

The short circuit analysis in the FeS is based upon the latest BC Hydro system model, which includes the generating facility information and associated impedance data provided by the IC. A more detailed study will be performed at the System Impact Study stage if needed.

5.3 Stations Requirements

[redacted] is expected to connect to the BC Hydro's existing 230kV Meikle Terminal Station (MKT). It is assumed that there is sufficient space to add associated P&C equipment in the existing MKT control building. The station upgrade scope at the existing Meikle Terminal Station (MKT) is as follows:

- Add one 230 kV Circuit Breaker (CB) and two disconnect switches to form a 4-CB ring bus inside the station fence.
- Add one 230 kV terminal, including a motor operated disconnect switch, a Capacitor Voltage Transformer (CVT), a Surge Arrester (SA) and associated busworks and supporting structures at MKT.
- Install associated P&C, station service and other equipment.
- Connect IC to the new 230 kV terminal at MKT.
- Upgrade station grounding system as necessary.

See Appendix C (Figure C-1) for stations planning partial one-line diagram showing the scope of work at MKT.

6 Cost Estimate and Schedule

The non-binding good faith estimated cost and time to construct the Network Upgrades required to interconnect the proposed project will be provided in a separate letter to the IC.

7 Conclusions

To interconnect the [redacted] and its facilities to the BCH Transmission System at the POI, this Feasibility Study has identified the following conclusions and requirements:

1. A new 230 kV line position is required at Meikle Terminal Station (MKT) to facilitate the interconnection of [redacted].
2. The connection of [redacted] does not cause any performance violation (i.e. thermal overload, voltage performance violation or voltage stability concern) under system normal conditions.
3. The connection of [redacted] will exacerbate the pre-existing thermal overload on the BC Hydro lines 2L308 and 2L312 and introduce a new overload on 2L309 under single contingencies or breaker contingencies. The [redacted] will be required to participate in the existing Peace Region Local Gen Shed RAS. The IC is also required to participate in GMS Area Gen Shed RAS for Peace 500 kV transmission line contingencies. Detailed Peace Region Local Gen Shed RAS and GMS Area Gen Shed RAS functional requirements modifications will be specified later if the IC's project proceeds to next stage of the interconnection process.
4. [redacted] is required to install anti-islanding protection within its facility to disconnect the IC's generating plant from the grid when an inadvertent island with the local load forms. The anti-islanding protection shall be configured in the manner that does not compromise the required ride-through performance.
5. The [redacted] is required to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range, per BC Hydro's TIR Section 6.4.2.
6. The "STATCOM option" for the proposed type-3 WTGs is required so that each turbine can provide reactive power capability at zero MW output. BC Hydro recognizes that Type-3 WTGs with the STATCOM option have an inherent limitation—providing only partial reactive power capability during turbine standstill.

7. Fast Frequency Response, also known as Virtual Inertia Control (VIC) in the proposed wind turbines is required at [redacted]
   The proposed wind turbine generators, when equipped with the VIC option, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The VIC settings should be determined in coordination with BC Hydro in the later stage of the interconnection process.

The above conclusions are made based on the IC's input data and study assumptions listed in Section 4, which represent the best available information on October 14, 2025.

Appendix A
Schematic Diagram of the IC's Project

Figure A-1 shows the schematic diagram for the [redacted]
Note that the proposed plant configuration includes 16 Mvar switchable shunt capacitor.

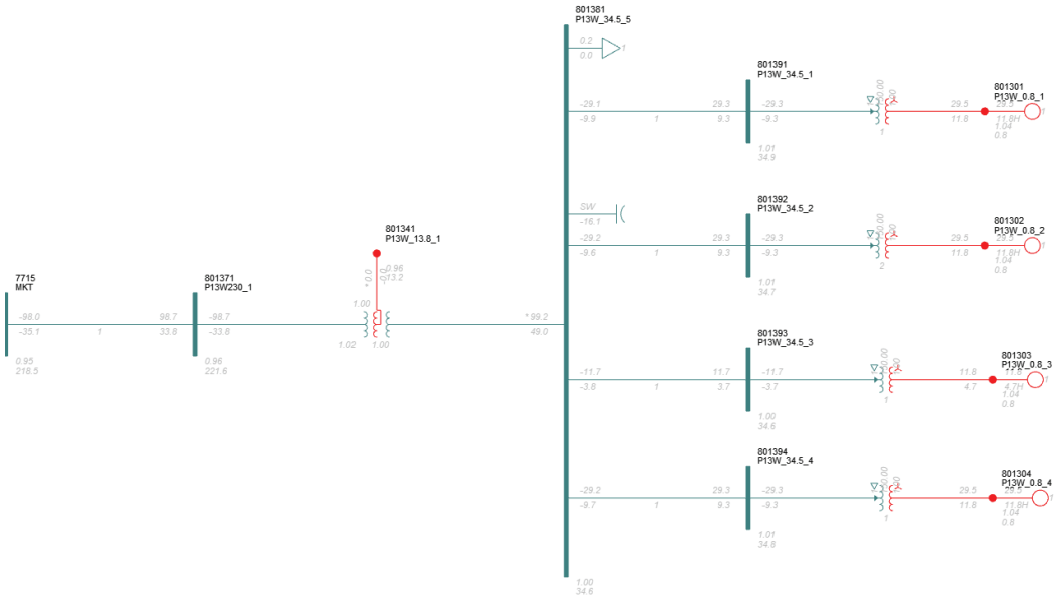

Figure A-1: [redacted] Plant Schematic Diagram.

Appendix B
Power Flow Study Results

Base Scenario (32HS, 32LS, 31HW)

Table B-1: Thermal Overload Study Results

Case	Peace Regional Generation	Contingency		Branch Loading (% of its seasonal normal rating)		
				2L308	2L309	2L312
		Cat.	Description	GMS-DKT	DKT-SNK	SNK-SLS
Summer Rating in MVA				427.5	427.5	424.7
32HS	Max	P0	System Normal			
	Max	P1.2	2L308			145%
	Max	P1.2	2L309			113%
	Max	P1.2	2L312	146%	114%	
	Max	P2.3	SLS 2CB11 OR 2CB12	146%	114%	
	Max	P2.3	SGB 2CB6, 2CB7, OR SLS 2CB14	119%		
	Max	P2.3	SNK 2CB12	124%		
	Max	P2.3	DKT 2CB2 OR 2CB3			113%
	Max	P2.3	DKT 2CB4			112%
Summer Rating in MVA				427.5	427.5	424.7
32LS	Max	P0	System Normal			
	Max	P1.2	2L308			145%
	Max	P1.2	2L309			113%
	Max	P1.2	2L312	146%	114%	
	Max	P2.3	SLS 2CB11 OR 2CB12	146%	114%	
	Max	P2.3	SGB 2CB6, 2CB7, OR SLS 2CB14	119%		
	Max	P2.3	SNK 2CB12	124%		
	Max	P2.3	DKT 2CB2 OR 2CB3			113%
	Max	P2.3	DKT 2CB4			112%
Winter Rating in MVA				541.4	539.4	538.2
31HW	Max	P0	System Normal			
	Max	P1.2	2L308			112%
	Max	P1.2	2L312	112%		
	Max	P2.2	SLS 2CB11 OR 2CB12	112%		

Table B-2: Steady-State Voltage Study Results

Case	IC's Plant Output	Contingency		Bus Voltage (PU)					
		Cat.	Description	DKT 230	GMS 230	MKT 230	SLS 230	SNK 230	TLR 230
31HW	Max	P0	System Normal	1.02	1.01	1.04	1.03	1.03	1.04
	Max	P1.2	2L312	0.99	0.98	1.03	1.04	1.00	1.04
32HS	Max	P0	System Normal	1.02	1.01	1.04	1.03	1.03	1.04
	Max	P1.2	2L312	0.98	0.98	1.03	1.04	1.00	1.04
32LS	Max	P0	System Normal	1.02	1.01	1.04	1.03	1.03	1.04
	Max	P1.2	2L312	0.98	0.98	1.03	1.04	1.00	1.04

Appendix C
Station Planning One-Line Sketch

Figure C-1 shows the Stations Planning partial one-line diagram and associated scope of work at the BC Hydro's existing 230kV Meikle Terminal Station (MKT).

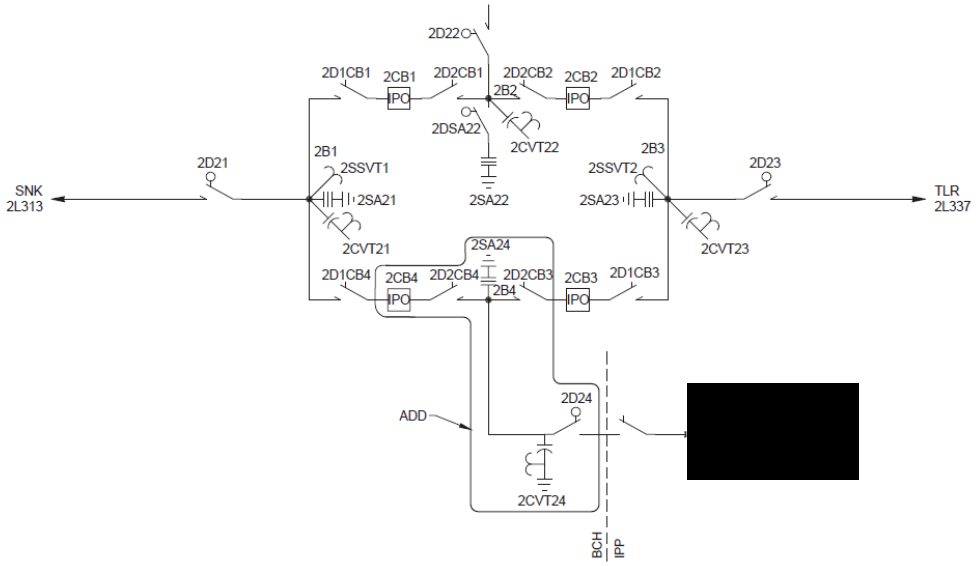

Figure C-1: Stations Planning - Partial One-Line Diagram with Scope of Work at MKT