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Burnaby, BC
V3N 4X8

November 24, 2025

[REDACTED]
[REDACTED]
[REDACTED]
[REDACTED]

via email: [REDACTED]

RE: CEAP IR #11 – [REDACTED] – Interconnection Feasibility Study

Dear [REDACTED]

Enclosed is the Interconnection Feasibility Study for the proposed Interconnection Request (IR), [REDACTED] submitted under Attachment M-2: Transmission Service and Interconnection Service Procedures for Competitive Electricity Acquisition Process (CEAP) of the Open Access Transmission Tariff (OATT). This letter provides a non-binding good faith estimate of the cost and time to construct the facilities required to interconnect your project to BC Hydro's Transmission System, being the Network Upgrades, based on the findings of the Interconnection Feasibility Study.

Open Access Transmission Tariff

The OATT defines Network Upgrades as additions, modifications, and upgrades to BC Hydro's Transmission System required at or beyond the Point of Interconnection to accommodate the interconnection of the Generating Facility to the BC Hydro's Transmission System. Pursuant to the OATT, BC Hydro will design, procure, construct, install, and own the Network Upgrades. While BC Hydro will pay the costs for the Network Upgrades, the Interconnection Customer provides security for such costs.

Interconnection Study Costs

The Interconnection Customer is responsible for paying the full cost of all Interconnection Studies in cash. Interconnection Study costs vary depending on the scope, complexity, and other factors such as whether any scope is shared with another Interconnection Customer (not applicable to this Interconnection Feasibility Study). The deposit amounts specified in the OATT are not proxy Interconnection Study costs. If actual Interconnection Study costs exceed the deposit amount, the Interconnection Customer must pay the remaining balance in cash. Please refer to the answer for question no. 53 in the posted [Questions & Answers for 2025 Call for Power](#) for typical study cost ranges.

Cost Estimate

Based on the Interconnection Feasibility Study, the non-binding good faith estimated cost (typical accuracy range of +150%/-50%) for Network Upgrades required to interconnect your project is \$239.4 M.

Major Scope of Work Identified:

- Expand BC Hydro Tumbler Ridge substation (TLR) to add one 230 kV line position with associated substation equipment
- Relocate the existing line terminal for 2L323 along with associated equipment at TLR and re-terminate on North side of substation
- Install new 230 kV line terminal with associated equipment at TLR
- Remove the temporary connection between bus 2B3 and 2B9
- Install one new 230kV circuit breaker and associated disconnects
- Upgrade required substation facilities, infrastructures, and bus work to support new station equipment
- Expand the existing 230kV switchyard within the limits of the current property boundaries.
- Thermal upgrades involving reconductoring of, and possible structure replacements of 230 kV line 2L313 from Meikle Wind station (MKT) to Sukunka station (SNK)
- Supply and install required Protection, Control and Telecommunications equipment

Exclusions:

- GST
- Permits
- Right-of-Way & property costs

Key Assumptions:

- Construction by contractor
- 24 months of construction is considered
- No construction during winter season
- Execution of early Engineering and Procurement Agreement
- No expansion of existing stations or control buildings to accommodate new equipment
- Impact Benefit Agreements with First Nations are not considered
- For the line thermal upgrade, 90% of the structures will be replaced, and reconductoring will be carried out

Key Risks:

- Expansion of the existing control building may be required leading to increased costs and/or a longer project schedule
- Major equipment delivery presents potential project cost and schedule risks, based on variance in equipment lead times
- No defined supply chain strategy; construction costs may increase depending on delivery method
- Project schedule may be longer than expected, leading to increased overhead costs
- Ground improvements may be required leading to increased construction costs
- Contaminated soil may be encountered leading to increased construction costs
- Cost of materials and major equipment may be affected by market conditions and escalation

Study Limitations and Exclusions

Protection, Control, and Telecommunications

The Interconnection Feasibility Study does not include a detailed review of the protection, control, and telecommunications system requirements specific to your Interconnection Request. Based on a high-level review, we have identified proxy costs for protection, control, and telecom Network Upgrades drawn from comparable interconnection projects with similar scope and complexity; these proxy costs have been included solely for indicative budgeting purposes. The relative interconnection cost determined by the Interconnection Feasibility Study includes a telecommunications component based on an assumed solution to deliver teleprotection and telecontrol circuit requirements necessary for the Interconnection Request. Protection, control, and telecommunications system requirements will be reviewed in detail in the System Impact Study if you are a successful participant of the CEAP and meet applicable requirements.

For Interconnection Feasibility Study purposes, it is assumed that any applicant-proposed works that could obstruct or impair the performance of existing BC Hydro microwave systems or new links from the proposed Interconnection Customer Interconnection Facilities (ICIF) to the BC Hydro microwave system would be identified and either relocated or repositioned as determined in a System Impact Study if you are a successful participant of the CEAP and meet applicable requirements. Such works may include, but are not limited to, towers, turbines, dams, support structures, panels, surface materials deposited or redistributed, water surface changes, or vegetation.

Generation Shedding/Curtailment Scheme and Electromagnetic Transient (EMT) Studies

The generation shedding/curtailment scheme reviews (e.g., Remedial Action Scheme (RAS), and a direct transfer trip for anti-islanding scheme) and EMT studies are completed in a System Impact Study. The outcomes of these studies may result in additional requirements, which could include Network Upgrades or ICIF. Any costs associated with completion of these studies, and resulting requirements, are not included in the Interconnection Feasibility Study cost estimate.

Revenue Metering

Please note that revenue metering requirements have not been determined with the Interconnection Feasibility Study. As such, any costs associated with revenue metering and other interconnection components are not included in the cost estimate provided above. Once these requirements are defined, costs that are attributable to the Interconnection Customer are to be paid in cash. For more details on revenue metering requirements and responsibilities, please refer to:

<https://www.bchydro.com/content/dam/BCHydro/customer-portal/documents/distribution/standards/ds-rmr-complex-revenue-metering.pdf>.

Schedule

Based on the Interconnection Feasibility Study, the non-binding good faith estimated in-service date for your Interconnection Request's Network Upgrades is Quarter 3 2033 (calendar year). To achieve this timeline, we may need to expedite certain activities, including engineering design and procurement of long-lead equipment.

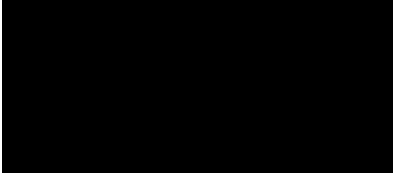
Timely actions required from you to minimize risks to the schedule:

- Submission of additional technical data required for the System Impact Study and Facilities Study
- Submission of any required information or document such as demonstration of Site Control
- Execution of Combined Study Agreement and Standard Generator Interconnection Agreement
- Financial commitments and securities

Please note that changes to your Interconnection Request or delays in data submission or financial commitments may also impact the target in-service date.

If you have any questions, please contact the BC Hydro CEAP team at ceap2025@bchydro.com.

Sincerely,



Manager, Customer Interconnections

BC Hydro

Encl.: CEAP_2025_IR11_  Feasibility_Study.pdf



Interconnection Feasibility Study

BC Hydro EGBC Permit to Practice No: 1002449

2025 CEAP IR # 11

Prepared for:



Prepared by:



Specialist Engineer, Transmission
Operations Services

Reviewed by:



Principal Engineer, Transmission
Operations Services

Accepted by:



Manager, Transmission Planning

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Prepared for: [REDACTED]
Prepared by: [REDACTED]
Title: Specialist Engineer, Transmission Operations Services
Checked by: [REDACTED]
Title: Specialist Engineer, Transmission Operations Services
Reviewed by: [REDACTED]
Title: Principal Engineer, Transmission Operations Services

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Revision	Date	Description
0	2025 Nov	Initial release

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Contributors

The following accept responsibility for the content in the specified sections. Professionals apply their signature and/or seal as appropriate.

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Entire report
except listed
below

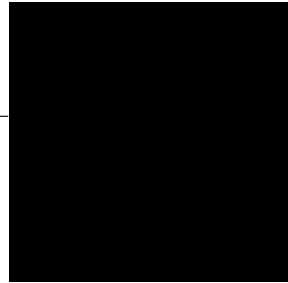
Discipline:

Transmission Operations Services

Contributed by:



Specialist Engineer, Transmission
Operations Services



Section:

5.2, 5.3

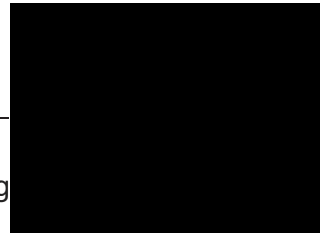
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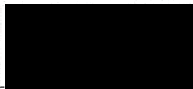
Section:

5.4

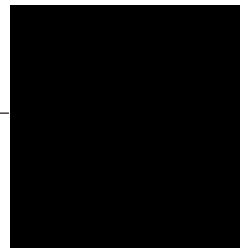
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Executive Summary

[REDACTED] the interconnection customer (IC), requests to interconnect its [REDACTED] (2025 CEAP IR #11) to the BC Hydro (BCH) system. [REDACTED] [REDACTED] has twenty-five (25) [REDACTED] type-3 wind turbine generators with a maximum power injection of 144.07 MW into the BC Hydro system at the Point of Interconnection (POI).. The proposed POI is at BC Hydro's 230 kV Tumbler Ridge substation (TLR). The IC's project will connect to the POI via a 24.48 km 230 kV interconnection line. The IC's proposed commercial operation date (COD) is February 5th, 2031.

To interconnect the [REDACTED] and its facilities to the BCH Transmission System at the proposed POI, this Feasibility Study has made the recommendations and conclusions as follow:

1. Relocating 2L323 line position and adding a new 230 kV line position with bus work modification and upgrades.
2. The connection of [REDACTED] will cause thermal overloading on 2L313 under system normal condition (N-0). Thermal upgrades on 2L313 from MKT to SNK is required by changing conductor from the existing SP 927.2 ASC to new ASC Columbine (at 90°C conductor temperature, 30°C ambient summer Temperature) with potential structure replacements.
3. The connection of [REDACTED] will exacerbate the pre-existing thermal overload on a few BC Hydro 230 kV lines under single contingencies. These overloads are presently addressed by the Peace Region generator shedding Remedial Action Scheme (RAS). It will also cause new thermal overloading on certain transmission lines or transformers under N-1 system contingency conditions. These new overloads can be resolved by modifying/expanding the existing Peace Region local wind farm generation shed RAS. The new wind generators at [REDACTED] are required to participate in this Peace Region Local Gen Shed RAS. The [REDACTED] [REDACTED] generators are also required to participate in GMS Area Gen Shed RAS for Peace 500 kV transmission line contingencies. Detailed Peace Region Local Gen Shed RAS and GMS

Area Gen Shed RAS functional requirements modifications will be specified later if the IC's project proceeds to the next stage of the interconnection process.

4. [REDACTED] is required to install anti-islanding protection within its facility to disconnect the IC's generating plant from the grid when an inadvertent island with the local load forms. The anti-islanding protection shall be configured in the manner that does not compromise the required ride-through performance.
5. [REDACTED] is required to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range, per BC Hydro's TIR Section 6.4.2.
6. The "STATCOM option" for the proposed type-3 WTGs is required so that each turbine can provide reactive power capability at zero MW output. BC Hydro recognizes that Type-3 WTGs with the STATCOM option have an inherent limitation—providing only partial reactive power capability during turbine standstill.
7. Fast Frequency Response, also known as Virtual Inertia Control (VIC) in [REDACTED] turbines, is required at the [REDACTED]. The proposed wind turbine generators, when equipped with the VIC option, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The VIC settings should be determined in coordination with BC Hydro in the later stage of the interconnection process.

The above conclusions are made based on the IC's input data and study assumptions listed in Section 4, which represent the best available information on October 14, 2025.

A non-binding good faith cost for required network upgrades and estimated schedule for construction are included in a separate letter to the IC.

Please note that, this Feasibility Study report does not include the descriptions of Protection, Control, and Telecommunications requirements and the associated upgrade scopes; However, as discussed in Section 2 "Purpose and Scopes of

Study, the associated cost implications are captured and delivered in the cover letter to the IC”.

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Appendices

Appendix A	Schematic Diagram of the IC's Project
Appendix B	Power Flow Study Results
Appendix C	TLR Station Planning One Line Diagram

Acronyms

The following are acronyms used in this report.

BCH	BC Hydro
CEAP	Competitive Electricity Acquisition Process
COD	Commercial Operation Date
DTT	Direct Transfer Trip
ERIS	Energy Resource Interconnection Service
FeS	Feasibility Study
IBR	Inverter-Based Resources
IC	Interconnection Customer
IR	Interconnection Request
IPP	Independent Power Producer
LAPS	Local Area Protection Schemes
MPO	Maximum Power Output
NERC	North American Electric Reliability Corporation
NRIS	Network Resource Interconnection Service
OATT	Open Access Transmission Tariff
POI	Point of Interconnection
RAS	Remedial Action Scheme
SBK	South Bank Substation
SIS	System Impact Study
TAY	Taylor Substation
TIR	BC Hydro “60 kV to 500 kV Technical Interconnection Requirements for Power Generators”
TLR	BC Hydro Tumbler Ridge Substation
VIC	Virtual Inertia Control
WECC	Western Electricity Coordinating Council
WTG	Wind Turbine Generator

1 Introduction

Table 1-1 below summarizes the project reviewed in this Feasibility Study.

Table 1-1 Summary of Project Information

Project Name	[REDACTED]	
Name of Interconnection Customer (IC)	[REDACTED]	
Point of Interconnection (POI)	Tumbler Ridge Substation (TLR)	
IC's Proposed COD	5 th February 2031	
Type of Interconnection Service	NRIS <input checked="" type="checkbox"/>	ERIS <input type="checkbox"/>
Maximum Power Injection (MW)	144.07 (Summer)	144.07 (Winter)
Number of Turbines	25 x 5.9 MW	
Plant Fuel	Wind	

[REDACTED] the interconnection customer (IC), requests to interconnect its [REDACTED] (2025 CEAP IR #11) to the BC Hydro (BCH) system. [REDACTED] [REDACTED] has twenty-five (25) [REDACTED] type-3 with a maximum power injection of 144.07 MW into the BC Hydro system at the Point of Interconnection (POI).. The POI is at BC Hydro's 230 kV Tumbler Ridge substation (TLR). The IC's project will connect to the POI via a 24.48 km 230 kV interconnection line. The IC's proposed commercial operation date (COD) is February 5th, 2031.

Figure 1-1 shows the Peace region 138/230/500 kV transmission system diagram. The Peace Regional System is connected to Peace 500 kV bulk transmission system through two 500 kV substations GMS and SBK:

- One 230 kV transmission line 2L308 and two 138 kV transmission lines 1L361 and 1L364 connecting GMS substation to Peace Regional system, and
- Two 230 kV transmission lines 2L391 and 2L392 and three 138 kV transmission lines 1L360, 1L370, and 1L374 connecting SBK substation to Peace Regional system, and

- Two 500 kV transmission lines 5L5 and 5L6 connecting SBK to PCN 500 kV substation, and through eight 500 kV transmission lines from GMS/PCN further down to BC Hydro load centre in the south.

[REDACTED] project is connecting to BC Hydro's 230 kV substation at Tumbler Ridge (TLR), as showing in Figure 1.1 below. Currently there are a few existing wind farm IPPs connected at Tumbler Ridge area such as DKW, ZBW, MKL, MLW, and QTY, so there are pre-existing branch overloading concerns under single or multiple contingencies. The Peace Region Local Wind Farm Generation Shedding RAS is relied on to address these overloading concerns.

There is a new wind farm project - [REDACTED] with installed capacity of 54.6 MW, to be connected at BC Hydro Sukunka substation. The in-service date for [REDACTED] is September 30th, 2030. The temporary station code [REDACTED] and its connection is shown in Figure 1-1 below.

In addition, there are two wind farm projects, which are also shown in Figure 1-1 below. Details about these two wind farms are as the following:

- [REDACTED] – 194 MW, tap connection on 2L391 at 28 km from SBK. In service date is October 1st, 2030
- [REDACTED] – 195.9 MW, a three-circuit breaker ring switching station loop in and out of 2L392 at 22 km from SBK. The in-service date is September 30th, 2031

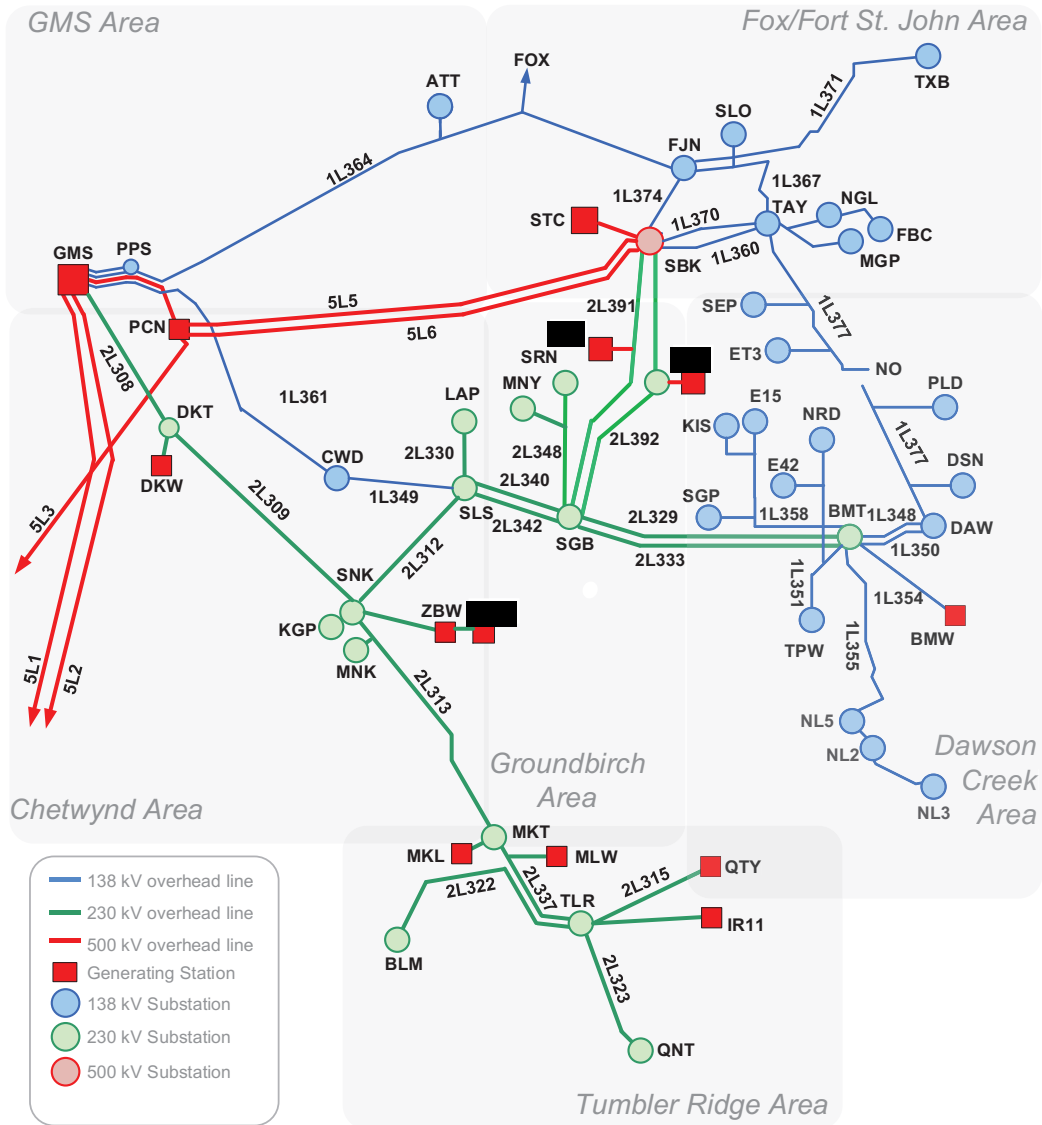


Figure 1-1: Peace Region 138/230/500 kV Transmission System Diagram

2 Purpose and Scopes of Study

This Feasibility Study is a preliminary evaluation of the system impact of interconnecting the proposed project to the BC Hydro system based on power flow and short circuit analysis in accordance with BCH's Open Access Transmission Tariff (OATT) and produces the estimated cost of required Network Upgrades and the implementation schedule.

Per OATT, the Feasibility Study is performed individually for each of the participating projects in the CEAP process and focuses specifically on the BC Hydro regional transmission system where the proposed generating project is connected and affects.

This is a "limited scope" study which is restricted to power flow studies of P0, P1 and P2 planning events as defined in TPL-001-4 and short circuit analysis. The study does not address other technical aspects such as transient stability and switching transients and impact of multiple contingencies. These subjects will be addressed in subsequent System Impact Study if the project proceeds further. In addition, any potential impacts to the adjacent external systems to BC Hydro would be addressed in subsequent detailed and coordinated studies with the relevant adjacent entities if the proposed generator project proceeds further.

Please note that, due to the compressed study timeline for 2025 CEAP Feasibility Study, this report does not include the descriptions of the Protection, Control, and Telecommunication requirements and the associated upgrade scopes. Instead, the network upgrades associated with Protections, Controls and Telecommunications are incorporated with cost estimates in a separate cover letter to the IC.

3 Standard and Criteria

The Feasibility Study is performed in compliance with the North American Electric Reliability Corporation (NERC) and Western Electricity Coordinating Council (WECC) reliability standards, and the BCH interconnection requirements in the TIR, and upon the ratings of the existing BCH transmission facilities described in Operating Orders, specifically:

- NERC standards: TPL-001-4 and FAC-002-3 relevant to the scope of this Feasibility Study.
- WECC criteria TPL-001-WECC-CRT-4 Transmission System Planning Performance, July 1, 2023.
- BC Hydro's 60 kV to 500 kV Technical Interconnection Requirements for Power Generators, Rev 2.1.1, Effective: Sept 22, 2025.
- BC Hydro Operating Order 5T-10, Ratings for All Transmission Circuits 60 kV or Higher, Sept 17, 2025.
- BC Hydro Operating Order 5T-14, Ratings for All Transmission and Distribution Transformer, Sept 22, 2025.
- BC Hydro System Operating Order 7T-22 System Voltage Control, Sept 19, 2023.

4 Assumptions and Conditions

This Feasibility Study is performed based on the IC's submitted data and information available to BC Hydro on Oct 14, 2025 for the study purpose. Assumptions are made wherever the IC's input is unavailable. Appendix A shows the schematic diagram of the IC's project used in the study model.

The power flow study cases used in this Feasibility Study are established based upon the BC Hydro's base resource plan and load forecasts available at the time of performing the study, which includes existing and future generators, transmission facilities, and loads in addition to the subject interconnection project in this study. Applicable seasonal conditions and the appropriate study years for the study planning horizon are also incorporated. Additional assumptions are listed as follows.

- 1) The generation in the study area are dispatched to the patterns that stress the transmission system in the study area. In these patterns, the associated generators are typically set to their Maximum Power Outputs (MPO) unless otherwise specified.
- 2) There are three new wind farm IPPs planned in the same area as this IC, all with similar in-service dates of between 2030 to 2031. See Section 1 for detailed information.
- 3) BMT T4 300 MVA has been planned to be in service by March 2027.
- 4) A new 138 kV transmission line from SBK to TAY - 1L370 has been planned to be in service by March 2029.

5 System Studies and Results

5.1 Power Flow Study Results

Power flow studies were performed to evaluate whether the IC's generating project would cause any unacceptable system performance (e.g. equipment overloads, steady-state voltage violation and voltage instability) and to determine the system reinforcement requirement based on steady state performance analysis.

The study focuses on the base scenario — 31HW/31LS/31HS system conditions that include [REDACTED] and [REDACTED] in Peace Region and the future proposed 1L370 between SBK to TAY, plus de-commission of MCM two units. These base cases were prepared based on factors such as load conditions, seasonal variation in ambient temperatures, and generation patterns that stress the transmission system.

In addition to the base scenario, an additional system condition of 32LS that includes [REDACTED] has been studied to cover the impact of high queue projects that enter into service after this IC.

The studies are performed for system normal conditions and under critical system contingencies specified in the P1 and P2 events by NERC TPL-001-4. Study results are summarized below.

5.1.1 Thermal Overload Analysis

The study has found thermal overloading on 2L313 under system normal condition , i.e. 106% loading on 2L313 MKT-MNK, 103.2% loading on 2L313 MNK-SNK. Thermal upgrades on 2L313 from MKT to SNK is required and summer 30 degree C ratings should be upgraded to at least 1250 A from the existing ratings of 1073 A (MNK – MKT)/1082 A (SNK – MNK). No other performance violations have been found under system normal condition, such as other thermal overload, voltage performance violation or voltage stability concern, caused by connection of [REDACTED]

The study has observed pre-existing branch overloads on 2L308, 2L309, and 2L312 under single contingencies (N-1 system conditions), i.e. 2L308 and/or 2L309 overloaded for loss of 2L312, or 2L312 overloaded for loss of 2L308 or 2L309. The connection of [REDACTED] will aggravate these pre-existing overloads, which is currently addressed by Peace

Region Local Gen Shed RAS. It will also cause new thermal overloading on certain transmission lines or transformers under other N-1 system conditions. These new overloads can be resolved by modifying/expanding the existing Peace Region local wind farm generation shed RAS scheme. The new wind generators at [REDACTED] [REDACTED] are required to participate in this Peace Region Local Gen Shed RAS.

In addition, [REDACTED] is also required to participate in GMS Area Gen Shed RAS scheme for Peace 500 kV transmission line contingencies.

Detailed Peace Region Local Gen Shed RAS and GMS Area Gen Shed RAS functional requirements modifications will be specified later if the IC's project proceeds to next stage of the interconnection process.

Please refer to Appendix B for detailed Power Flow Study results.

5.1.2 Steady-State Voltage Analysis

With the connection of the IC's project, the steady-state voltage performance under system normal condition (P0) is acceptable for all the studied load conditions (31HW/31LS/31HS/32LS).

5.1.3 Reactive Power Capability Evaluation

The BC Hydro TIR requires IBR power plant to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range.

Based on the power flow model data submitted by the IC, the proposed [REDACTED] [REDACTED] would be capable of meeting the BC Hydro's reactive capability requirement at the plant's maximum MW output, which is subject to further verification in the next stage of the call process.

In addition, according to the IC-provided reactive capability data, the proposed WTG would provide +1.7 Mvar to -1.9 Mvar reactive capability at the zero MW output if the turbine's "STATCOM" function is enabled. This function needs to be re-confirmed if the IC's project proceeds to next stage of the interconnection process.

5.1.4 Anti-Islanding Requirements

[REDACTED] is not arranged for islanded operation. In addition, the IC is required to install anti-islanding protection within its facility to disconnect the IC's wind farm from the grid when an inadvertent island with the local loads forms.

5.1.5 Other Performance Requirements

Fast Frequency Response, also known as Virtual Inertia Control (VIC) in [REDACTED] wind turbines, is required at the Sundance Wind Project Tumbler Ridge POI 147 MW. The proposed wind turbine generators, when equipped with the VIC option, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The VIC settings should be determined in coordination with BC Hydro in the later stage of the call process.

5.2 Fault Analysis

The short circuit analysis in the Feasibility Study is based upon the latest BC Hydro system model, which includes the generating facility information and associated impedance data provided by the IC. A more detailed study will be performed at the System Impact Study stage if needed.

5.3 Stations Requirements

To interconnect the [REDACTED] Interconnection Customer (IC) to BC Hydro's transmission system at the 230 kV bus of the Tumbler Ridge (TLR) Substation the following station works are required:

- Relocate the existing line terminal 2L323 along with associated equipment - 2CVT4 and 2D24, so that the line egress is from the north side of the substation. With the addition of the seventh circuit breaker (2CB2) as part of the interconnection at the TLR substation, the total number of circuit breakers now exceeds the planning criteria for typical "ring" bus configuration. Therefore, provisions must be made for a future circuit

breaker (2CB10) to complete a meshed ring configuration. However, no additional circuit breaker will be installed under this project, apart from the relocation of the 2L323 line terminal and its associated equipment.

- Remove the temporary connection between bus 2B3 and 2B9.
- Install one new outdoor dead-tank type, 230kV circuit breaker (2CB2) rated at 3000A continuous current, 40kA interrupting rating, 950kV BIL along with associated disconnects rated 3000A.
- Install a new 230kV line terminal (2LXXX- Sundance Wind Project) with associated motorised disconnect switch (2D23) rated 3000A, Surge Arrester (2SA13) and one 230kV Capacitor Voltage Transformer (2CVT3).
- Expand the existing 230kV switchyard within the limits of the current property boundaries to accommodate the above-mentioned facilities.
- Install associated protection and control (P&C) equipment and other equipment.
- Other associated station works.
- Refer to the one-line diagram Appendix C for details.

5.4 Transmission Line Requirements

- Thermal upgrades on 2L313 from MKT to SNK from existing 1073 A (MNK – MKT)/1082 A (SNK – MNK) to required 1250 Amps (30°C ambient summer Temperature) by conductor changing from the existing SP 927.2 ASC to new ASC Columbine (at 90°C conductor temperature, 30°C ambient summer Temperature) with structure replacements may be required. In the case of planned outage constrain of 2L313, build a brand new parallel circuit with the new proposed replacement conductor and new right-of-way may be required.
- Re-terminate 2L323 to the north side of the TLR substation.

6 Cost Estimate and Schedule

The non-binding good faith estimated cost and time to construct the Network Upgrades required to interconnect the proposed project will be provided in a separate letter to the IC.

7 Conclusions

To interconnect the [REDACTED] and its facilities to the BCH Transmission System at the POI, this Feasibility Study has identified the following conclusions and requirements:

1. Relocating 2L323 line position and adding a new 230 kV line position with bus work modification and upgrades
2. The connection of [REDACTED] will cause thermal overloading on 2L313 under system normal condition (N-0). Thermal upgrades on 2L313 from MKT to SNK is required by changing conductor from the existing SP 927.2 ASC to new ASC Columbine (at 90°C conductor temperature, 30°C ambient summer Temperature) with potential structure replacements.
3. The connection of [REDACTED] will exacerbate the pre-existing thermal overload on a few BC Hydro 230 kV lines under single contingencies. These overloads are presently addressed by the Peace Region generator shedding Remedial Action Scheme (RAS). It will also cause new thermal overloading on certain transmission lines or transformers under N-1 system contingency conditions. These new overloads can be resolved by modifying/expanding the existing Peace Region local wind farm generation shed RAS. The new wind generators at [REDACTED] are required to participate in this Peace Region Local Gen Shed RAS. The [REDACTED] generators are also required to participate in GMS Area Gen Shed RAS for Peace 500 kV transmission line contingencies. Detailed Peace Region Local Gen Shed RAS and GMS Area Gen Shed RAS functional requirements modifications will be specified later if the IC's project proceeds to the next stage of the interconnection process.
4. [REDACTED] is required to install anti-islanding protection within its facility to disconnect the IC's generating plant from the grid when an inadvertent island with the local load forms. The anti-islanding protection shall be configured in the manner that does not compromise the required ride-through performance.

5. The [REDACTED] is required to have the dynamic reactive power capability at a minimum of +/- 33% of its MPO at the high voltage side of the IC's switchyard over the full MW operating range, per BC Hydro's TIR Section 6.4.2.
6. The "STATCOM option" for the proposed type-3 WTGs is required so that each turbine can provide reactive power capability at zero MW output. BC Hydro recognizes that Type-3 WTGs with the STATCOM option have an inherent limitation—providing only partial reactive power capability during turbine standstill.
7. Fast Frequency Response, also known as Virtual Inertia Control (VIC) in [REDACTED] wind turbines, is required at the [REDACTED]. The proposed wind turbine generators, when equipped with the VIC option, are expected to temporarily boost the MW output to limit the system frequency drop during a major frequency event. The VIC settings should be determined in coordination with BC Hydro in the later stage of the interconnection process.

Appendix A Schematic Diagram of the IC's Project

Figure A-1 shows the schematic diagram for the [redacted] [redacted]. Note that the proposed plant configuration includes a 24 MVAR switchable shunt capacitor on collector bus.

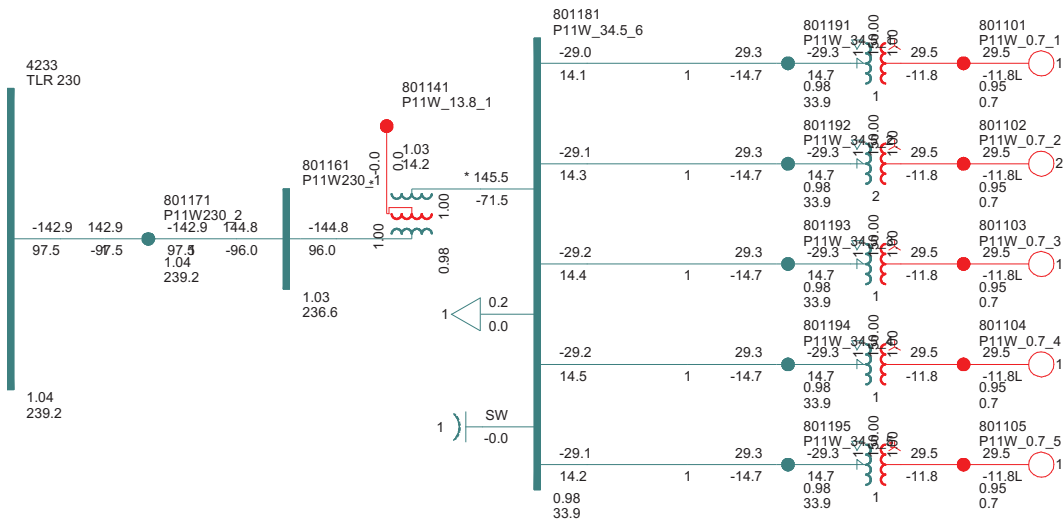


Figure A-1: [redacted] Schematic Diagram.

Appendix B

Power Flow Study Results

Table B-1: Summary of Branch Loading Study Results

Study Case - 32LS								
Peace Regional Generation/ Load	IC's Generator Output	Contingency Identified		Branch Loading (MVA)				
				2L308 DKT	2L309 SNK	2L312 SNK	2L313 MKT	GMS T13
		Category	Description	GMS-DKT	DKT-SNK	SNK-SLS	SNK-MKT	GMS 500/230 kV
5514 MW / 1000 MW	147.5W	P0	System Normal	381.6	245.1	285.2	453	172
				89.26%	57.33%	67.15%	105.96% (Note 1)	57.33%
		P1.2	2L308 OOS		-139.1 -32.54%	668.9 157.50%	452.5 90.86% (Note 2)	-17 -5.67%
		P1.2	2L309 OOS	-139.8 -32.70%		530.2 124.84%	452.8 90.92% (Note 2)	53 17.67%
		P1.2	2L312 OOS	648.7 151.74%	529.3 123.81%		452.8 90.92% (Note 2)	300.9 100.30%
		P1.2	2L392-1 SBK to [REDACTED]	433.1 101.31%	298.5 69.82%	231.8 54.58%	452.9 90.94% (Note 2)	197.2 65.73%
		P2.3	SBK 2CB21 or 2CB22 (loss of 2L392-1 SBK to [REDACTED] & (SBK T21 or SBK T22)	447.8 104.75%	313.8 73.40%	216.4 50.95%	452.9 90.94% (Note 2)	204.4 68.13%
		P2.2	GMS T14&T12	347.5 81.29%	209.9 49.10%	320.4 75.44%	453 90.96% (Note 2)	309.7 103.23%

Note 1: Based on the existing summer 30 degree C rating of 1073 A (427.5 MVA)

Note 2: Based on the upgraded summer 30 degree C rating of 1250 A (498 MVA)

Appendix C

One-Line Diagram for Planned TLR Substation

Figure C-1 shows the Stations Planning One-Line Diagram for the Proposed Changes at TLR

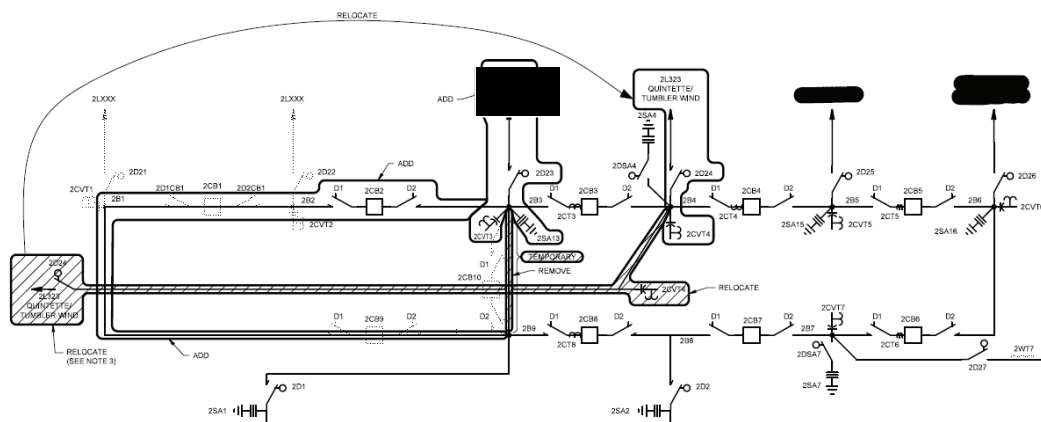


Figure C-1: TLR Station Planning One-Line Diagram for IR11